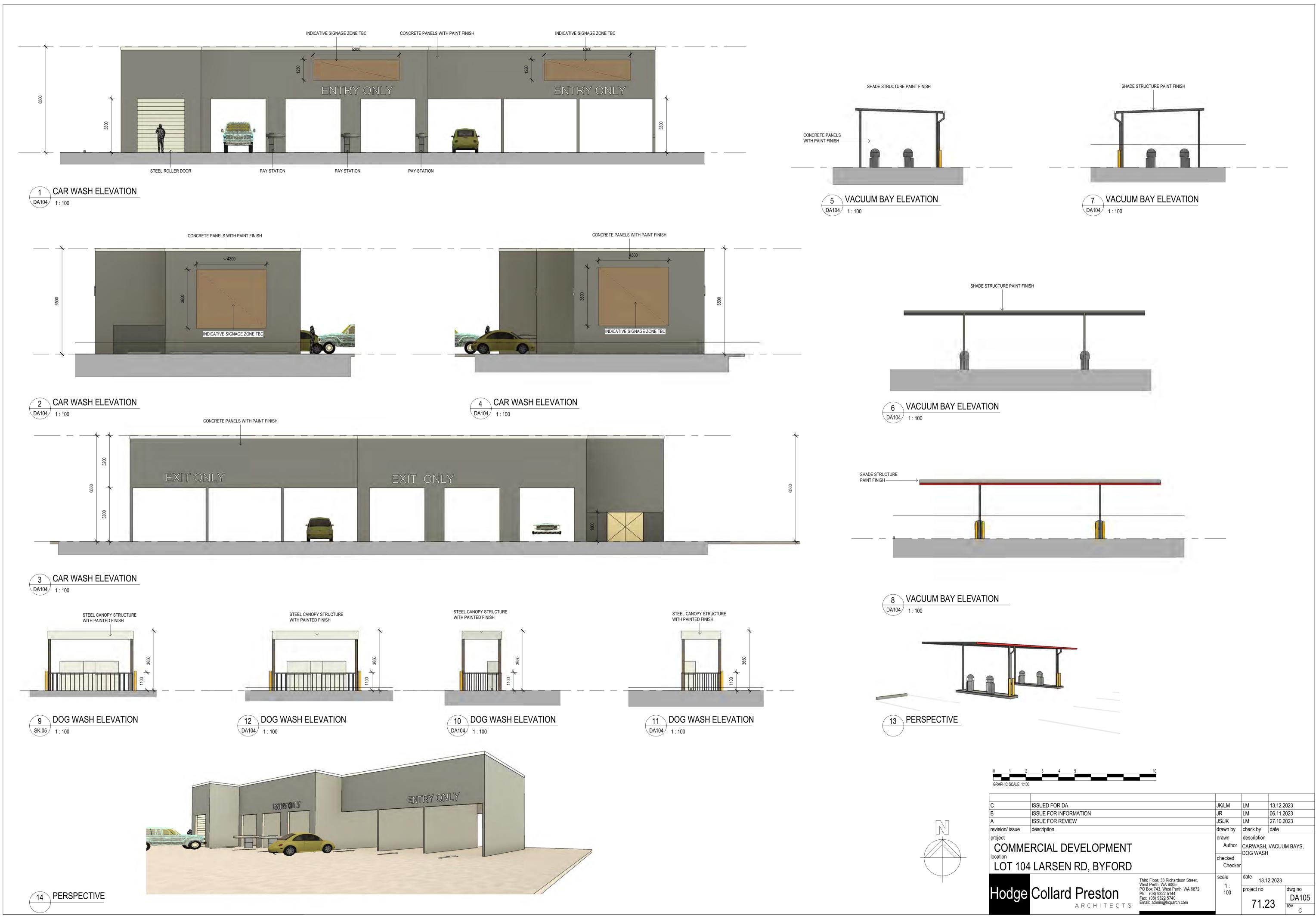
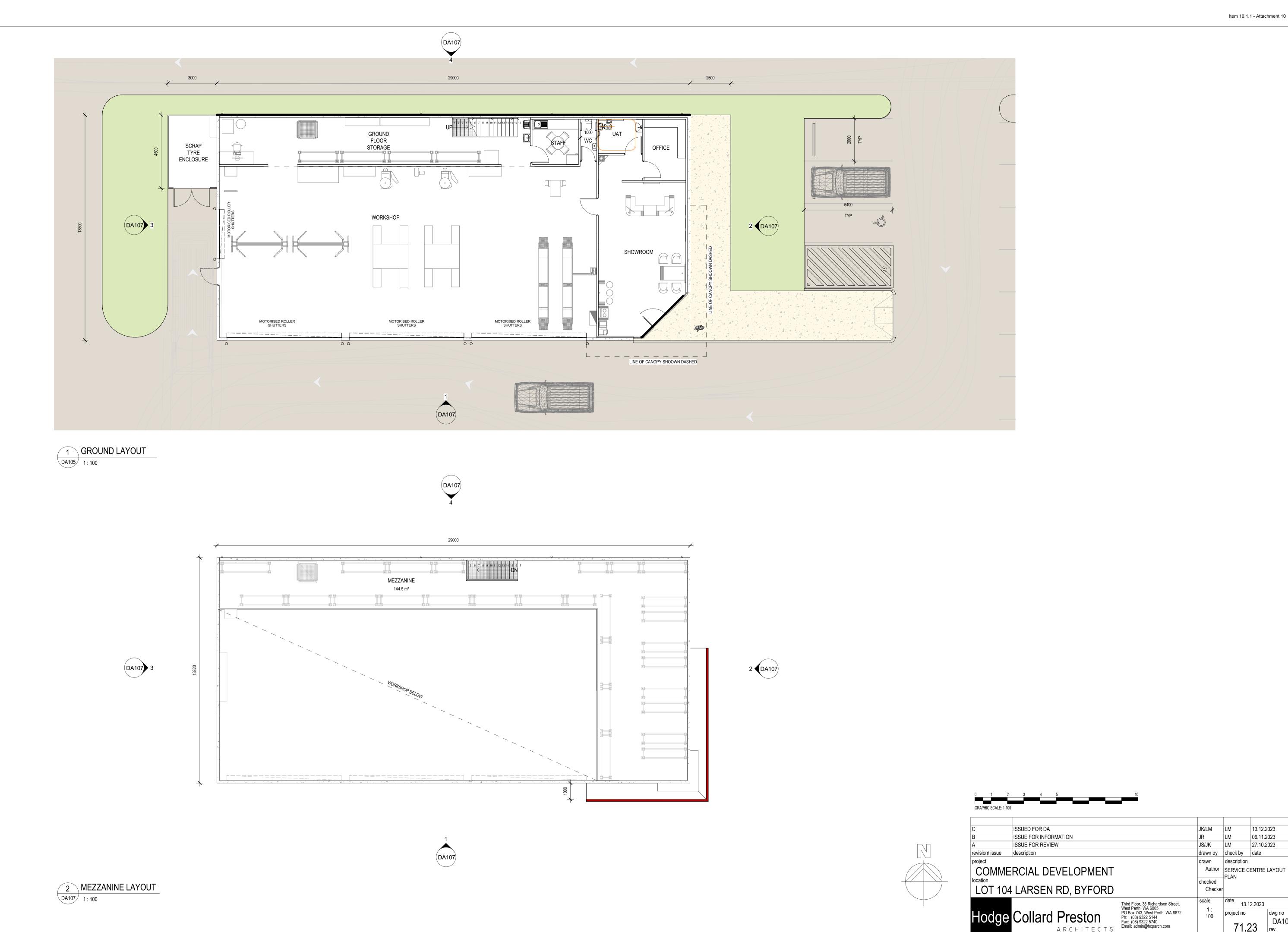


2 VACUUM BAYS PLAN
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1 CARWASH PLAN
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Hodge	Collard Preston	PO Box 743, West Perth, WA 6872 Ph: (08) 9322 5144 Fax: (08) 9322 5740 Email: admin@hcparch.com	100	project no 71.2	dwg no





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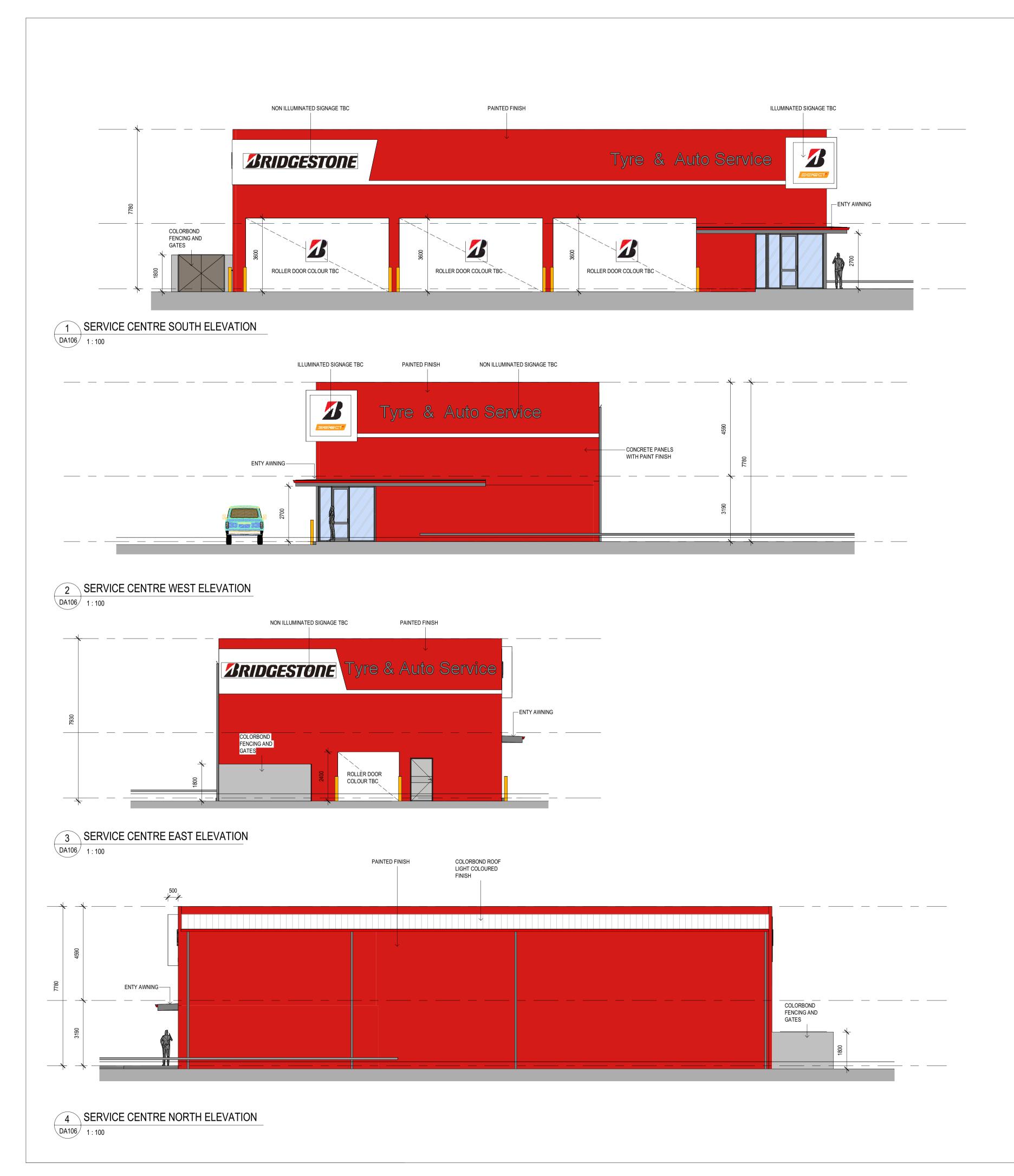
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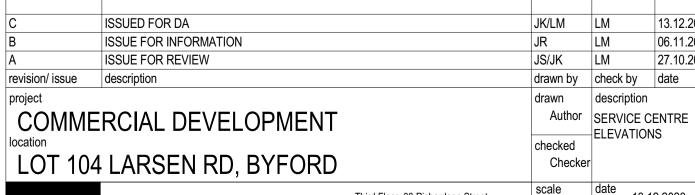
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5 SERVICE CENTRE 3D VIEW





Third Floor, 38 Richardson Street, West Perth, WA 6005 PO Box 743, West Perth, WA 6872 Ph: (08) 9322 5144 Fax: (08) 9322 5740 Email: admin@hcparch.com

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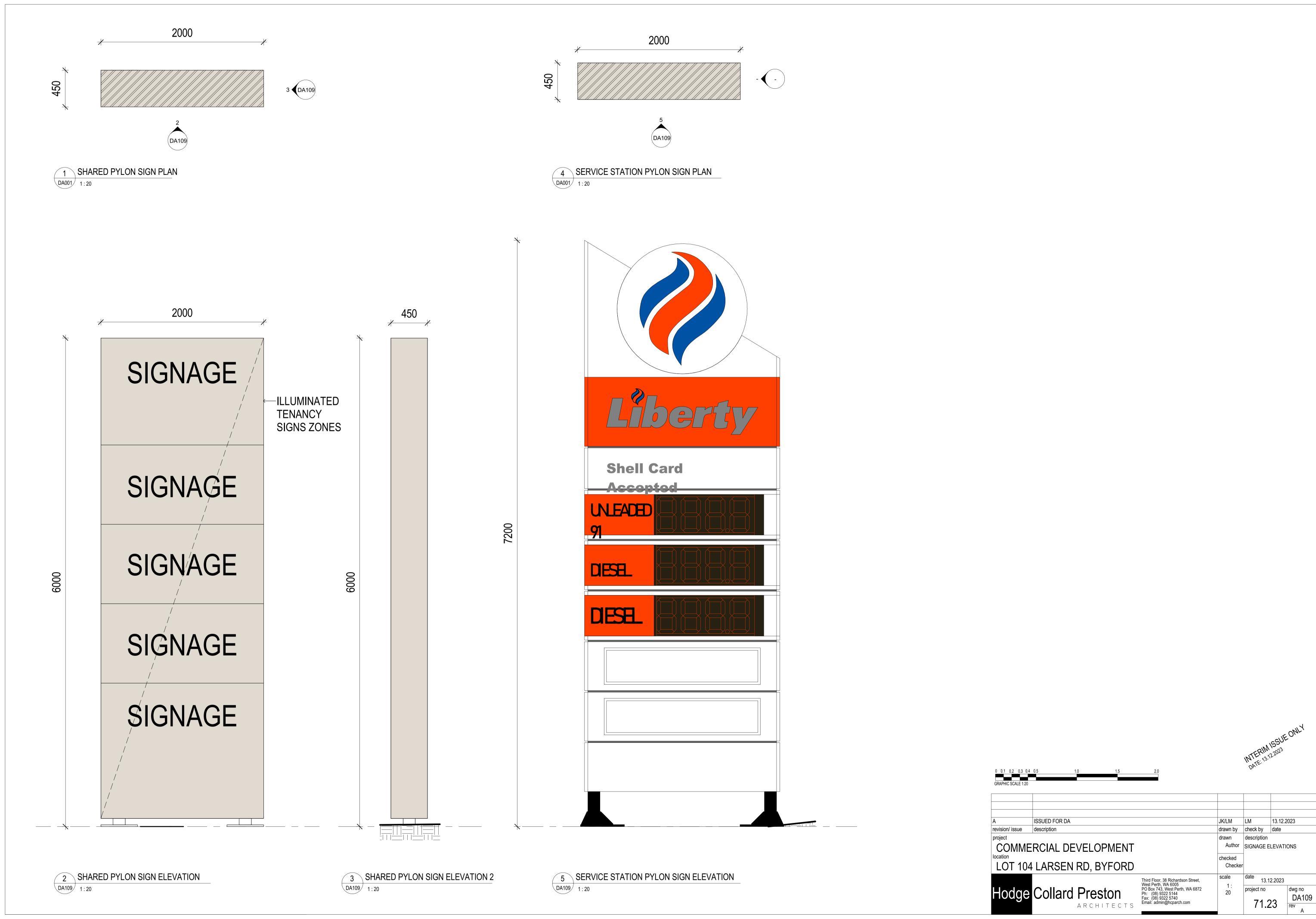
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# Proposed Commercial Development

Lot 104 (No 3) Larsen Road, Byford Transport Impact Assessment



## **Document history and status**

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**Project:** 3 Larsen Road, Byford

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## 1 Introduction

This Transport Impact Assessment (TIA) has been prepared by Transcore on behalf of Capital Prudential with respect to the proposed commercial development to be located at 3 Larsen Road, Byford in the Shire of Serpentine-Jarrahdale (Shire).

The subject site is approximately 11,635m<sup>2</sup>. It is bound by Larsen Road to the north, South Western Highway (SWH) to the east, George Street to the west and existing developments to the south as shown in Figure 1.



Figure 1: Location of the subject site

The key issues that will be addressed in this report include the traffic generation and distribution of the proposed development, review of the existing and proposed site crossovers and capacity analysis of the development crossovers and intersection of South Western Highway and Larson Road as a network.

The location of the subject site within the *Metropolitan Region Scheme (MRS)* context is illustrated in **Figure 2**. Review of the *MRS* identifies South Western Highway as a "Primary Regional Road" under care and control of Main Roads WA and all other roads surrounding the subject site are local roads under care and control of the Shire. The subject site is zoned as "*Urban*" in the *MRS*.

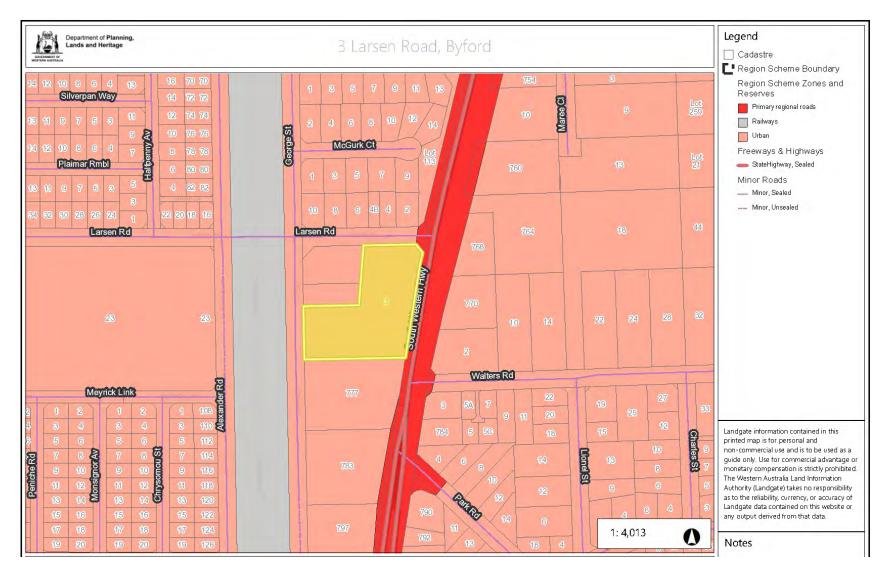


Figure 2: Location of the subject site within the MRS

## 2 Development Proposal

The proposal is for construction of a commercial development comprising the following elements:

- Fast Food Outlet 1 with Drive-through: 220m² GFA;
- Fast Food Outlet 2 with Drive-through: 250m<sup>2</sup> GFA;
- Service Centre: 400m<sup>2</sup> GFA;
- Car Wash: 3 manual bays plus 3 auto bays;
- Dog wash:1 bay;
- Service Station: 300m<sup>2</sup> convenience store plus 8 light vehicle fill points.

The site currently has one full movement crossover on SWH. The intention is to retain the existing full-movement crossover on SWH without any modifications and add one full movement crossover on Larsen Road and another one on Geroge Street to create an efficient accessibility and circulation system and distribute the development traffic satisfactorily on the surround roads and intersections. Figure 3 shows the location of the existing and proposed crossovers. The site layout has been reviewed to ensure efficient and satisfactory movement of various vehicles entering and exiting the site (refer Appendix B).

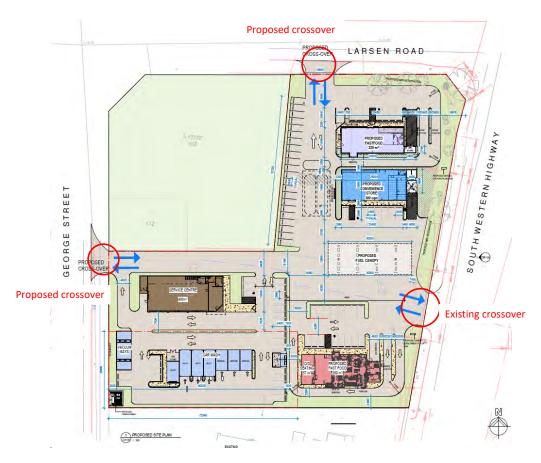


Figure 3: Existing and proposed crossovers

## 3 Existing Situation

## 3.1 Existing Road Network

The existing road hierarchy and standard of the surrounding roads are presented in Figure 4.

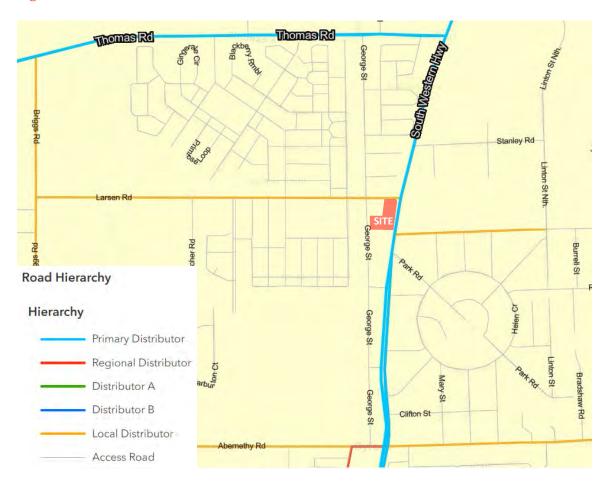


Figure 4: Existing road hierarchy

**South Western Highway** (SWH) is classified as a *Primary Distributor* in the Main Roads WA *Functional Road Hierarchy*. It is also classified as a *Primary Regional Road* (i.e. a red road) in the *Metropolitan Region Scheme*. SWH is under the care and control of Main Roads WA and operates under the sign-posted speed limit of 60km/h in the vicinity of the subject site.

The existing SWH reserve width is approximately 35m in the vicinity of the site and reduces to 30m past Walters Road. This section is constructed as an 11m-wide two-lane single carriageway road. It has a 2m shared path within both verges. It forms a full movement T-intersection with Larsen Road at the northeast corner of the site and at Walters Road south of the site. Basic widening is in place on SWH at Larsen Road intersection to allow for through movement on SWH to pass the right turning vehicles from SWH to Larsen Road. This intersection also entails a left turn lane on SWH.



Figure 5: South Western Highway looking south at Larsen Road intersection

**Larsen Road** is classified as a *Local Distributor* in the Main Roads WA *Functional Road Hierarchy*. Larsen Road operates under the default built-up area speed limit of 50km/h.

The existing road reserve width is approximately 20m and is constructed as a 9m-wide single-carriageway two-lane road. Larsen Road has a 2m shared path on the southern side of the road. It forms a T-intersection with South Western Highway at its eastern end and a four-way intersection with George Street in the west, adjacent to an existing railway crossing of Armadale Line railway.



Figure 6: Larsen Road looking west towards the existing railway crossing

**George Street** is classified as an *Access Road* in the Main Roads WA *Functional Road Hierarchy*. George Street operates under the default built-up area speed limit of 50km/h with 6.2m carriageway and 2m shared path on the eastern side.



Figure 7: George Street looking south at Larsen Road

George Street is currently constructed for approximately 290m south of Larsen Road (adjacent to the subject site) but is not yet constructed through to Evans Way south of the site. Georger Street is then constructed from Evans Way to Abernethy Road.

## 3.2 Existing Traffic Volume on Roads

The existing daily traffic counts obtained from Main Roads WA are presented in **Figure 8**. The traffic counts survey conducted by Matrix on September 2021 for Main Roads WA provides the peak hour counts at the intersection of SWH/Larsen Road. This survey by Matrix also included queue counts and delay surveys, which have been utilised for the calibration of the SIDRA analysis of the intersection. The available peak hour traffic counts at the intersections Larson Road with George Street and SWH are presented in **Figure 9**.

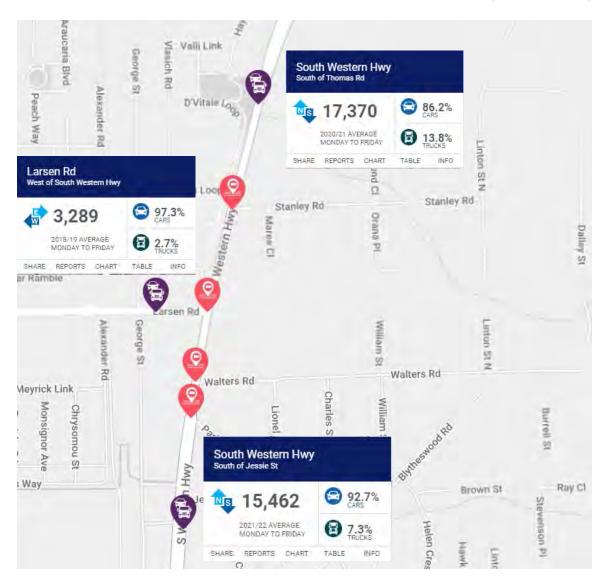


Figure 8: Existing daily traffic counts (Source: Main Roads WA)



Figure 9: Existing traffic 2021 counts AM/ PM peak hour

## 3.3 Public Transport Access

Existing bus routes in the vicinity of the subject site are presented in **Figure 10**. The closest bus stops are located on SWH to the north and south of the site.

Planning work is underway to extend the Armadale Line approximately 7 kilometres south of the existing Armadale Station with a new station at Byford. This new station is planned to be located between Evans Way and Clara Street (south of the subject site) and will include facilities such as Park N Ride (P n R), Kiss N Ride (K n R), a new bus interchange, as well as a cyclist/pedestrian path network connecting to and from the station complex (refer **Figure 11**). As part of this new station the existing railway crossing at Larsen Road will be closed and a new railway crossing at Clara Street will be constructed. It is understood that George Street will also be constructed through to Evans Way south of the site as part of this Metronet project.

It is expected that the current bus routes being operated by Transperth would respond to the new station and new growth areas in the vicinity.

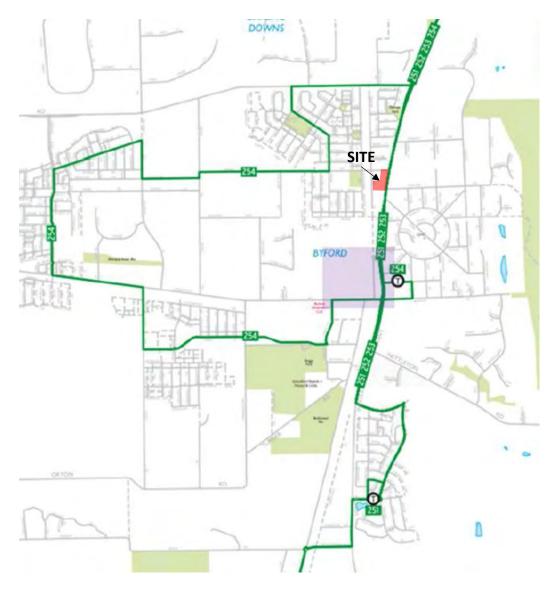


Figure 10: Existing bus services



Figure 11: Location of the new Byford station and new railway crossing in the vicinity

## 3.4 Pedestrian and Cyclist Facilities

The existing bicycle facilities (as at 2021), are shown in **Figure 12**, which is taken from the Department of Transport's *Perth Bike Map* series.

According to this map a high-quality shared path exists along George Street.



Figure 12: Bike map (source: Department of Transport)

## 3.5 Crash Data

The Main Roads WA website includes *summary crash history* data for all roads and intersections that recorded crashes over the 5-year period ending 31 December 2022.

Review of the crash history at SWH/ Larsen Road indicates a total of 2 rear end crashes at the intersection. No crashes were reported at Larsen Road/ George Street intersection.

# 4 Changes to Surrounding Transport Networks

Proposed changes to the surrounding road network as part of the Metronet Project are shown in Figure 13.



#### Legend

- Closure of existing railway crossing at Larsen Rd.
- New railway crossing at Clara St.
- George St connection Larsen Rd to Evans Way.
- 4. Sansimeon Blvd connection

Figure 13: Proposed changes in the surrounding road network

The proposed relocation of the railway level crossing from Larsen Road further south to Clara Street would remove most of the existing traffic along Larsen Road towards SWH. Review of the 2018 traffic counts at the 4-way intersection of Larsen Road/ George Street indicates that more than 80% of the traffic on Larsen Road between George Street and SWH is generated by the residential areas to the west of George Street and less than 20% was generated from the residential area to the north of Larsen Road.

# 5 Integration with Surrounding Area

The proposed development is of a commercial/retail character and is expected to address the existing and future demand for this type of services within Byford and specifically within this locality. The proposed land uses are in line with existing and future land uses that are located between SWH and Goerge Street in this locality.

## **6 Traffic Assessment**

## **6.1 Assessment Period**

Due to the nature of the development, it is expected that the greatest demand on the local road network capacity will be experienced during the combined peak hour of business activity of the development and the commuter traffic activity during the weekday morning and afternoon periods.

The assessment year that is adopted for the analysis is 2025. It is understood that Byford Station would be constructed in the near future, which would reduce the car mode share in the immediate locality and may change the traffic pattern due to the new park and ride facility. Further, due to capacity issues for this section of SWH, Tonkin Highway is anticipated to be extended south in the short-to-medium term (within 10 years) and as a result the traffic patterns and volumes on SWH will change. Therefore, due to the uncertainty about the future status and traffic volumes on SWH,10-year post development assessment is not undertaken in this instance.

## 6.2 Trip Generation and Distribution

#### 6.2.1 Service Station with Convenience Store – Regular Fuelling Points

Based on the feedback received from a number of Western Australia service station operators that the trip rates published in the Institute of Transportation Engineers 11th Edition Trip Generation Guidelines (a US trip generation source) significantly overestimate the actual patronage numbers, Transcore undertook extensive traffic surveys during 2022. As part of this survey, a total of 15 service stations were surveyed, in order to establish more accurate local traffic generation rates for this type of land use in Western Australia. All of the sites selected entailed different operators in order to ensure robust data with a high level of confidence. The surveys were undertaken on Mondays, Tuesdays and Wednesdays in order to include trade activity during the discounted fuel days as well and to ensure a conservative approach.

The following sites were surveyed for the purpose of the study:

7-Eleven, 194 Great Eastern Hwy, Ascot WA
Ampol, 204 Great Eastern Hwy, Ascot WA
BP, 1 Canham Way, Greenwood WA
BP, 88 Gilbertson Road, Kardinya WA
BP, 848 Canning Hwy, Applecross WA
Coles Express, 73A Frobisher Street, Osborne Park WA
Puma, 58 Montana Crescent, Alkimos WA
Ampol 3, Morwell Street, Yanchep WA
Liberty, 2341 Albany Highway, Gosnells WA
7-Eleven, 931 Wanneroo Road, Wanneroo WA
7-Eleven, 13 Lakes Road, Greenfield WA

Shell, 582 Stirling Highway, Mosman WA Puma, Cnr Johnson Street & Helena Street, Guildford WA United, 2 Feilman Drive, Leda WA United, 101 Terrier Place, Southern River WA

Accordingly, the trip rates which were used to estimate the traffic generation for the service station component of the proposed development are as follows:

Weekday daily: 162.20vpd per filling point;

Weekday AM peak hour: 9.49vph per filling point; and, Weekday PM peak hour: 11.27vph per filling point.

#### 6.2.2 Proposed fast-food outlets

ITE 11 was used to estimate the trip generation of the proposed fast-food outlets. The fast-food outlet 1 (220m²) with drive through facility is expected to serve breakfast but the fast-food outlet 2 (250m²) would not serve breakfast and is expected to generate less traffic compared to a high-traffic-generating fast-food outlet. Therefore, fast food outlet 2 was assumed to generate minimal traffic in the morning peak hour and about 70% of the trip rates suggested by ITE 11 Guidelines for fast-food outlet with drive through during the PM peak hours.

### Fast-food Outlet with drive through facility (#934)

Weekday daily: 503 vehicles per day per 100m<sup>2</sup> GFA;

Weekday AM peak hour: 48 vehicles per day per 100m<sup>2</sup> GFA; and, Weekday PM peak hour: 36 vehicles per day per 100m<sup>2</sup> GFA.

#### 6.2.3 Proposed service centre

ITE 11 was used to estimate the trip generation of the proposed service centre. Accordingly, the following trip rates were sourced (ITE 943):

Weekday daily: 18 vehicles per day per 100m<sup>2</sup> GFA;

Weekday AM peak hour: 2 vehicles per day per 100m<sup>2</sup> GFA; and, Weekday PM peak hour: 2 vehicles per day per 100m<sup>2</sup> GFA.

#### 6.2.4 Proposed car wash traffic generation

The trip rates for a car wash in ITE 11 appear to be unreasonably high for the road network peak hours. For example, for automatic car wash the trip rate is equivalent to one car being washed every 46 sends of the entire peak hour, which is clearly unreasonable. Accordingly, the traffic volumes likely to be generated by the proposed car wash were estimated based on projected customer numbers and number of staff and the information available in Transcore's database for similar land use.

Accordingly, the trip generation of the proposed manual and auto car wash are estimated as below:

#### Manual Car Wash

Weekday AM peak hour: 6 trips per hour per bay; Weekday PM peak hour: 6 trips per hour per bay; and,

Weekday: 60 trips per day per bay.

#### **Auto Car Wash**

Weekday AM peak hour: 15 trips per hour per bay; Weekday PM peak hour: 15 trips per hour per bay; and,

Weekday: 150 trips per day per bay.

#### 6.2.5 Proposed dog wash traffic generation

In the absence of any trip rates, it is conservatively assumed than one customer would use the dog wash every 20 minutes of the peak hour and therefore three customers per hour would utilise the proposed dog wash. This translates to the below trip generation during the road network peak hour:

Weekday AM peak hour: 6 trips per hour; Weekday PM peak hour: 6 trips per hour; and;

Weekday: 64 trips per day;

Data source and other assumptions are as follows:

- Directional splits of 50% in / 50% out assumed for all land uses as they are all dominated by customer arrival / departure except Service Centre which 72%/28% was assumed for AM peak hour and 39%/61% was assumed for PM peak hour (In accordance with ITE handbook).
- Pass-by rates were sourced from ITE Trip Generation Handbook 3rd Ed: Service Station with Convenience Market (#945): 62% for AM and 56% for PM (average of 60% for both peak hours were used). Fast-Food outlets (#933 and #934): 50%/ 50% for weekday AM and PM peak hours.
- Conservatively, 0% pass-by rate was assumed for the other land uses (Service Centre, Dog Wash, Auto Car Wash and Manual Car Wash).
- Fast-Food outlet 2 (250m² GFA) is not expected to be open in AM peak hour, therefore, zero trips was assumed for the AM peak hour.

**Table 1** shows the trip generation of the proposed development. The passing trade and primary trips associated with the proposed development are summarised in **Table 2**.

Due to the land use mix within the proposed development, incidences of multipurpose trips<sup>1</sup> (i.e., cross-trade) are anticipated. Accordingly, the applied cross-trade adjustment is calculated to result in a moderate overall reduction in trip generation of approximately 20% (In accordance with RTA NSW – Guide to Traffic Generating Developments) but only during the PM peak period and for overall daily trips.

Accordingly, it is estimated that the proposed development would generate a total of about 3,261 daily trips (both inbound and outbound) with about 207vph and 248vph during the weekday AM and PM peak hours respectively.

The distribution of traffic to and from the proposed development for year 2025 (post development) was established by considering the catchment area of the proposed development as well as the available access and egress routes to and from the site. It should be noted that by year 2025 or full development of the site it is assumed that the existing railway crossing at Larsen Road would be closed and the section of George Street between Larsen Road and Evans Way would be constructed. **Figure 14** shows the available access and egress routes to and from the site.

Consequently, the directional distribution of primary and passing traffic to and from the site is assumed to be as follows:

#### Primary trip distribution:

- 40% of all traffic to/from north direction (SWH);
- 30% of all traffic to/from south direction (SWH); and
- 30% of all traffic to/from Geroge Street.

#### Passing trip distribution:

- 35% of all traffic to/from north direction (SWH);
- 45% of all traffic to/from south direction (SWH); and
- 20% of all traffic to/from Geroge Street.

The distribution of the proposed development traffic is illustrated in Figure 15 for the AM and PM peak hours.

-

<sup>&</sup>lt;sup>1</sup> Multi-purpose trips are incidences where more than one shop/outlet are visited within the development (also referred to as "cross-trade")



Figure 14: Available access and egress routes to and from the site in 2025

Table 1: Weekday daily, morning, afternoon peak hours trip generation for the proposed land uses

Source	Land Use	Quantity	Daily Rate	AM Peak	PM Peak	Cross trade	Daily Trips	AM Trips	PM Trips	AM		PM	
Jource										IN	OUT	IN	OUT
ITE 943	Service Centre	400	0.18	0.02	0.02	20%	57	7	7	5	2	3	4
Transcore	Automated car wash	3	150	15	15	20%	360	36	36	18	18	18	18
Transcore	Manual car wash	3	60	6	6	20%	144	14	14	7	7	7	7
Transcore	Service station + Convenience store	8	162.20	9.49	11.27	20%	1038	61	72	30	30	36	36
ITE 934	Proposed Fast food	250	5.03	0.00	0.26	20%	1006	0	51	0	0	26	26
ITE 934	Proposed Fast food	220	5.03	0.48	0.36	20%	886	85	63	42	42	31	31
Transcore	Dog Wash	1	64.00	6.00	6.00	20%	51	5	5	2	2	2	2
_	Total						3542	207	248	105	102	123	125

Table 2: Passing trade and primary trip components of the trip generation

**Passing Trade Component** 

Passing Trade			Daily	Α	М	PM		
Daily	AM	PM	Daily	IN	OUT	IN	OUT	
0%	0%	0%	0	0	0	0	0	
0%	0%	0%	0	0	0	0	0	
0%	0%	0%	0	0	0	0	0	
60%	60%	60%	623	18	18	22	22	
50%	50%	50%	503	0	0	13	13	
50%	50%	50%	443	21	21	16	16	
0%	0%	0%	0	0	0	0	0	
	Total		1569	39	39	51	51	

**Primary Trips** 

- /										
A	М	PM								
IN	OUT	IN	OUT							
5	2	3	4							
18	18	18	18							
7	7	7	7							
12	12	14	14							
0	0	13	13							
21	21	15	15							
2	2	2	2							
66	63	72	74							
	1N 5 18 7 12 0 21 2	AM OUT 5 2 18 18 7 7 12 12 0 0 21 21 2 2	AM       PI         IN       OUT       IN         5       2       3         18       18       18         7       7       7         12       12       14         0       0       13         21       21       15         2       2       2							

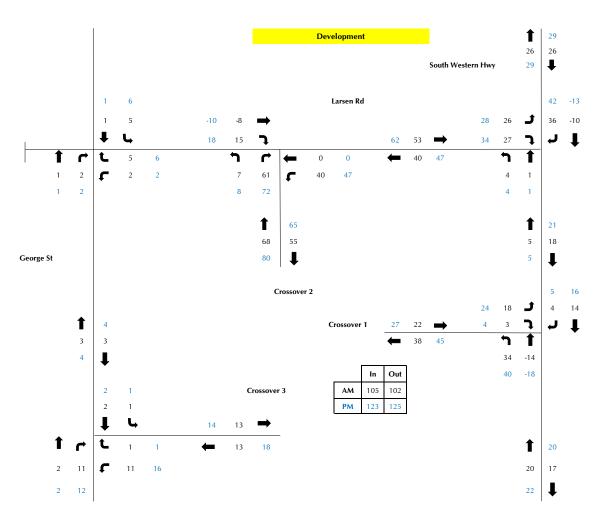


Figure 15: Development trip distribution during the AM and PM peak hours

### **6.3 Traffic Flow Forecasts**

The existing peak hour traffic counts on surrounding roads and intersections were established by traffic counts sourced from Main Roads WA (refer **Figure 8**). It is anticipated that existing railway crossing at Larsen Road would be closed and Clara Street crossing will open before the full development of the site and therefore, the existing base traffic on Larsen Road would reduce after the closure.

**Figure 13** illustrates the existing traffic on the surrounding road network in 2025 after closure of the railway crossing. A 2% per year traffic growth rate was applied to the background traffic to establish the 2025 traffic on SWH and George Street.

The total post development traffic for the assessment year was calculated with the base 2025 background traffic plus the development traffic.

The total projected traffic volumes for the assessment year are presented in **Figure** 16.

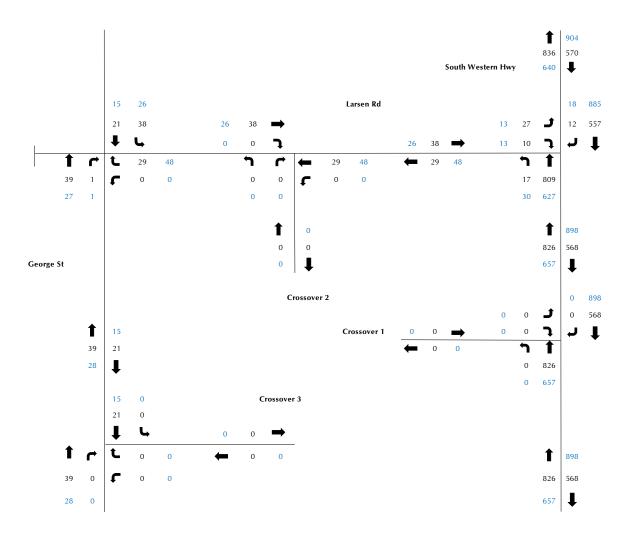


Figure 16: Total 2025 base traffic (after closure of railway crossing without development traffic) – AM Weekday and PM Weekday peak hours

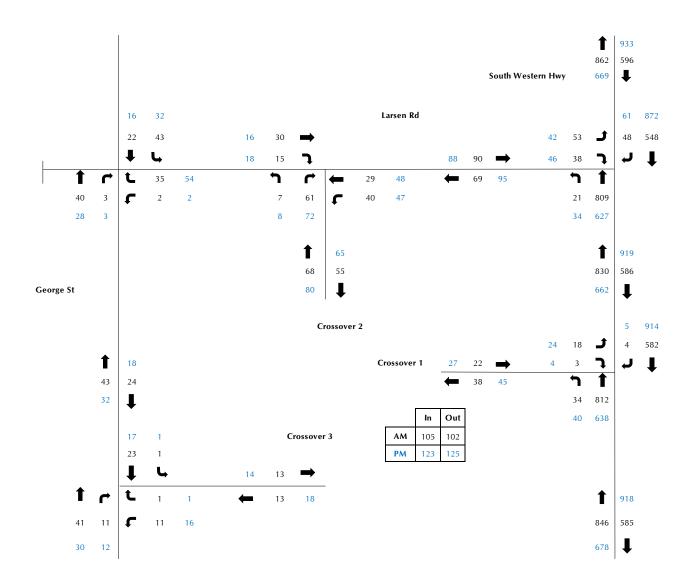


Figure 17: Total (2025 with development) traffic - AM Weekday and PM Weekday peak hours

### 6.4 Analysis of Local Intersections & Crossovers

Capacity analysis of the development crossovers and intersection of Larson Road/SWH was undertaken using the SIDRA computer software package. SIDRA is an intersection modelling tool commonly used by traffic engineers for all types of intersections. SIDRA outputs are presented in the form of Degree of Saturation, Level of Service, Average Delay and 95% Queue. These characteristics are defined as follows:

**Degree of Saturation** is the ratio of the arrival traffic flow to the capacity of the approach during the same period. The Degree of Saturation ranges from close to zero for infrequent traffic flow up to one for saturated flow or capacity.

**Level of Service** is the qualitative measure describing operational conditions within a traffic stream and the perception by motorists and/or passengers. In general, there are 6 levels of service, designated from A to F, with Level of Service A representing the best operating condition (i.e. free flow) and Level of Service F the worst (i.e. forced or breakdown flow).

**Average Delay** is the average of all travel time delays for vehicles through the intersection.

95% Queue is the queue length below which 95% of all observed queue lengths fall.

The results of the SIDRA analysis are summarised in Appendix C. Figure C1 in Appendix C shows the network layout modelled in SIDRA. The SIDRA intersection models were coded with reference to Main Roads WA Operation Modelling Guidelines. All relevant parameters such as heavy vehicle groups, PCU factors etc. were coded as per the Main Roads WA Guidelines.

#### **SWH/ Larsen Road intersection**

The SIDRA analysis results and site observations indicate that the intersection of SWH/ Larsen Road presently operates at capacity with level of service F for the critical right turn movement out of Larsen Road during both weekday peak hours. The gap acceptance and follow up parameters in SIDRA were adjusted slightly for this movement to calibrate the 2021 queues and delays at the intersection. **Figure 3** summarises the calibrated queues and delays at the intersection for the critical right turn movement out of Larsen Road.

Table 3: Sidra results for the critical movement at the SWH / Larsen Rd intersection in 2021

		Movement: Right tur	n out from Larsen Rd	
	Observe	d (2021)	Modele	d (2021)
	AM	PM	AM	PM
95% back of queue (Veh)	5.3	4.6	5.6	3.3
Average delay time (S)	68	52	69.2	54.7
LoS	F	F	F	F

The closure of the railway crossing at Larsen Road and the addition of the development-generated traffic to the intersection resulted in less traffic at the intersection in 2025 compared to 2021 and consequently minor decreases in overall queues and delays are reported. No change in overall LoS for the intersection is reported. Table 4 summarises the performance parameters for the critical right turn movement out of Larsen Road in 2025.

Table 4: Sidra results for the critical movement at the SWH / Larsen Rd intersection in 2025

	Movement: Right tui	n out from Larsen Rd
	2025 After road closure	and with development
	AM	PM
95% back of queue (Veh)	2.3	2.3
Average delay time (S)	58.7	57.2
LoS	F	F

#### **Development crossovers**

SIDRA analysis indicates that the existing SWH crossover and proposed development crossover on Larson Road will operate satisfactorily in 2025 during assessed peak hours. All movements operate with acceptable levels of service with minimal delays and queuing. The reported LOS for the critical right turn movement out of SWH crossover is reported as E in 2025 with less than one vehicle queue at the crossover. The reported queue for the right in movement from SWH into the crossover is less than one vehicle.

Notwithstanding that the SIDRA has reported maximum of only one vehicle queue for the right turn into the SWH crossover, Sk17a in Appendix B indicates that currently the width of SWH southbound at the existing crossover is sufficient to accommodate up to three B99 vehicles stopped on SWH to turn right into the crossover. This allows another vehicle to bypass the queue without colliding with the stationary vehicles.

Due to minimal traffic projections, George Street development crossover has not been assessed in SIDRA.

#### **Network Operations**

Relevant SIDRA network outputs were reviewed for assessed peak hours to establish the operation of the SWH/ Larsen Road intersection and development crossovers as an integrated network.

As detailed in Figure 18 there are no queue backs from the SWH/ Larsen Road intersection to the existing and proposed development crossovers on SWH and Larsen Road. Similarly, no queue backs from the development crossovers to SWH intersection is reported.

Hence, the capacity analysis confirms that the proposed development will not have an adverse impact on the operation of the local road network and that the proposed development crossovers will operate satisfactorily.

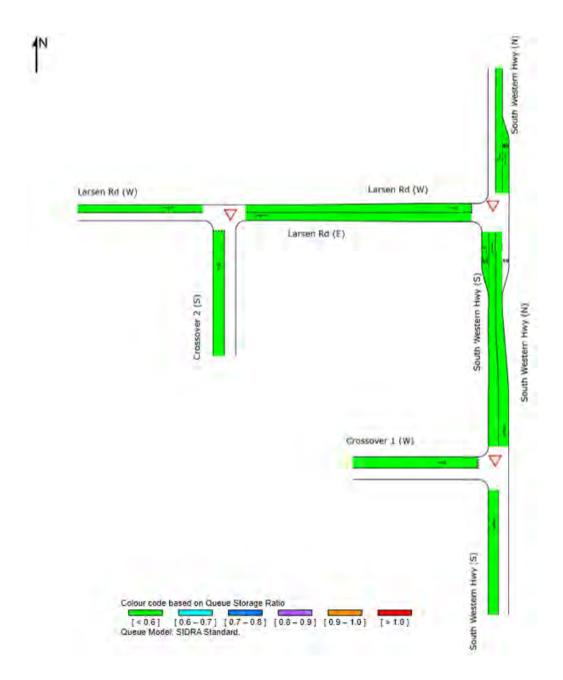


Figure 18: Critical weekday AM/PM peak hour network analysis – queue storage ratio (2025)

# 6.5 Impact on Surrounding Roads and Neighbouring Areas

The WAPC Transport Impact Assessment Guidelines (2016) provides the following guidance on the assessment of traffic impacts:

"As a general guide, an increase in traffic of less than 10 percent of capacity would not normally be likely to have a material impact on any particular section of road, but increases over 10 percent may. All sections of road with an increase greater than 10 percent of capacity should therefore be included in the analysis. For ease of assessment, an increase of 100 vehicles per hour for any lane can be considered as equating to around 10 percent of capacity. Therefore, any section of road where development traffic would increase flows by more than 100 vehicles per hour for any lane should be included in the analysis."

The proposed development will not increase traffic flows near the quoted WAPC threshold on the surrounding roads and therefore the traffic impact on surrounding roads are considered to be insignificant.

### 6.6 Traffic Noise and Vibration

It generally requires a doubling of traffic volumes on a road to produce a perceptible 3dB(A) increase in road noise. The proposed development will not increase traffic volumes or noise on surrounding roads near this level.

# 7 Parking

The proposed parking provision for the proposed development consists of 75 on-site parking spaces (including three ACROD bays). The parking supply calculation does not include the waiting bays within drive-through facilities and the bays under the service station canopy.

It is considered that the proposed parking provision is adequate to meet the parking demand of the proposed development.

# 8 Provision for Service Vehicles

There will be a number of service vehicles servicing the different land uses within the proposed development as outlined below:

#### **Service station**

A 19.0m fuel tanker is likely to deliver fuel to the proposed service station. The tanker is anticipated to turn right from SWH into Larson Road and then enter the site using the proposed crossover on Larsen Road and leave the site through the George Street crossover, heading north towards the Laren Road/George Street intersection. From there, the fuel tanker will proceed to exit onto SWH in the southbound direction.

A 12.5m service truck would be able to service the loading dock of the proposed convenience store. The proposed 12.5m truck would follow the same path as the fuel tanker to enter and exit the site.

#### **Fast Food Outlets**

The fast-food outlet 1 (220m² GFA) is expected to be serviced by 8.8m service vehicles, while fast-food outlet 2 (250m² GFA) would be serviced by a 12.5m service vehicle. Both the 8.8m and 12.5m service trucks will have the ability to enter the site using either the existing crossover on SWH or the proposed crossover on Larson Road. They will exit the site using the same crossovers.

#### **Service Centre**

An 8.8m truck would be able to enter and exit the proposed service bay of the service centre. The service vehicle would be able to enter and exit the site via the existing SWH crossover or the proposed Larson Road crossover.

#### Carwash

An 8.8m truck would be able to service the car wash as shown by the turn path plan. The service vehicle would be able to enter and exit the site via the existing SWH crossover or the proposed Larson Road crossover.

Turn path analysis undertaken for 19.0m fuel tanker, 12.5m and 8.8m service vehicles (refer **Appendix B**) indicate satisfactory movements.

# 9 Conclusions

This Transport Impact Assessment (TIA) has been prepared by Transcore on behalf of Capital Prudential with respect to the proposed commercial development to be located at 3 Larsen Road, Byford in the Shire of Serpentine-Jarrahdale.

The site currently has one full-movement crossover on SWH. The plan is to keep this existing crossover without any modifications and add two new crossovers on Larsen Road and Geroge Street. This will ensure efficient accessibility and circulation and satisfactory distribution of development traffic on the surrounding road network.

The proposed relocation of the railway level crossing from Larsen Road further south to Clara Street would remove most of the existing traffic along Larsen Road towards SWH. This will provide spare capacity on Larsen Road and its intersection with SWH. As part of this project George Street between Larson Road and Evans Way will also be constructed.

It is assumed that Larson Road rail crossing closure and George Street construction will occur by the time the proposed development is fully operational. This timeframe is assumed to be 2025.

It is understood that Byford Station would be constructed in the near future, which would reduce the car mode share in the immediate locality and may change the traffic pattern due to the new park and ride facility. Further, Tonkin Highway is anticipated to be extended south in the short-to-medium term (due to capacity issues along this section of SWH) and as a result the traffic volumes and pattern on SWH will change, with an expected reduction. Therefore, due to the uncertainty about the future status and traffic volumes on SWH,10-year post development assessment is not undertaken in this instance.

The SIDRA analysis results and 2021 traffic turn counts undertaken for Main Roads WA indicate that the intersection of SWH/ Larsen Road presently operates at capacity with level of service F for the critical right turn movement out of Larsen Road during both weekday peak hours.

The closure of the railway crossing at Larsen Road and the addition of the development-generated traffic to the intersection is estimated to result in less traffic at the intersection in 2025 compared to 2021 and consequently minor decreases in overall queues and delays are reported by SIDRA.

SIDRA analysis indicates that the existing and proposed development crossovers will operate satisfactorily in 2025 during assessed peak hours. All movements operate with acceptable levels of service with minimal delays and queuing.

It is concluded that the findings of this Transport Impact Statement are supportive of the proposed development.

# **Appendix A**

**PROPOSED DEVELOPMENT PLANS** 



Engineering a better future for over 20 years!

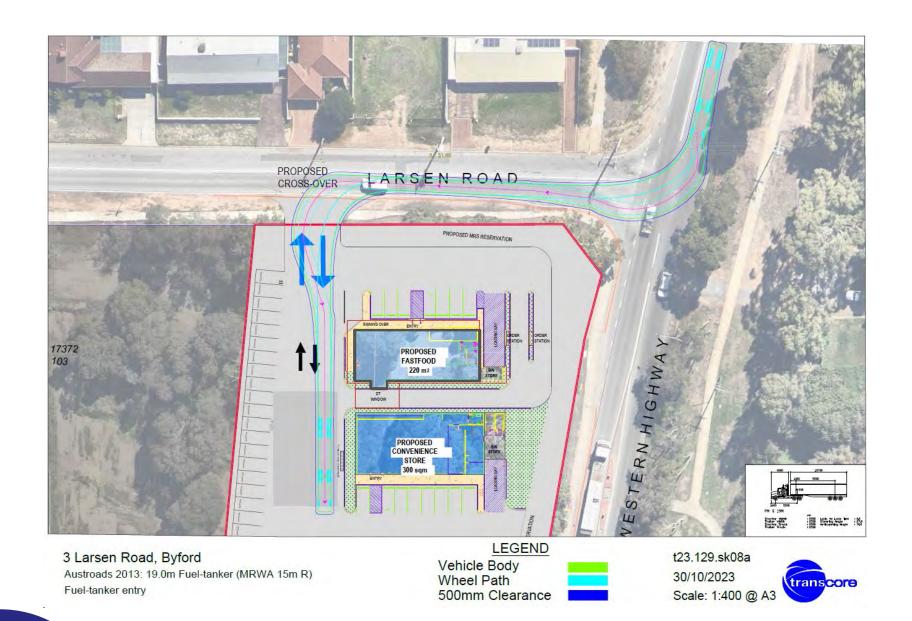


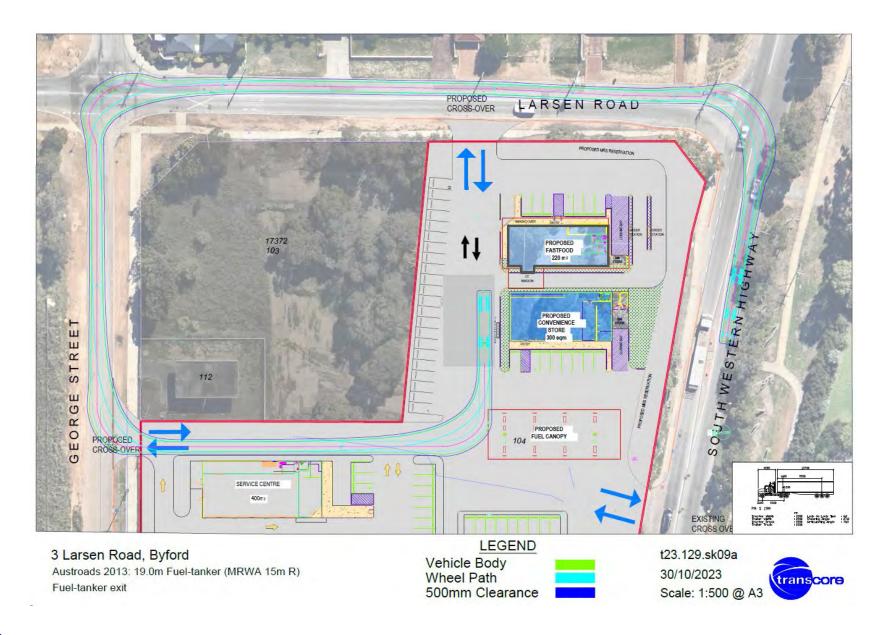
# Appendix B

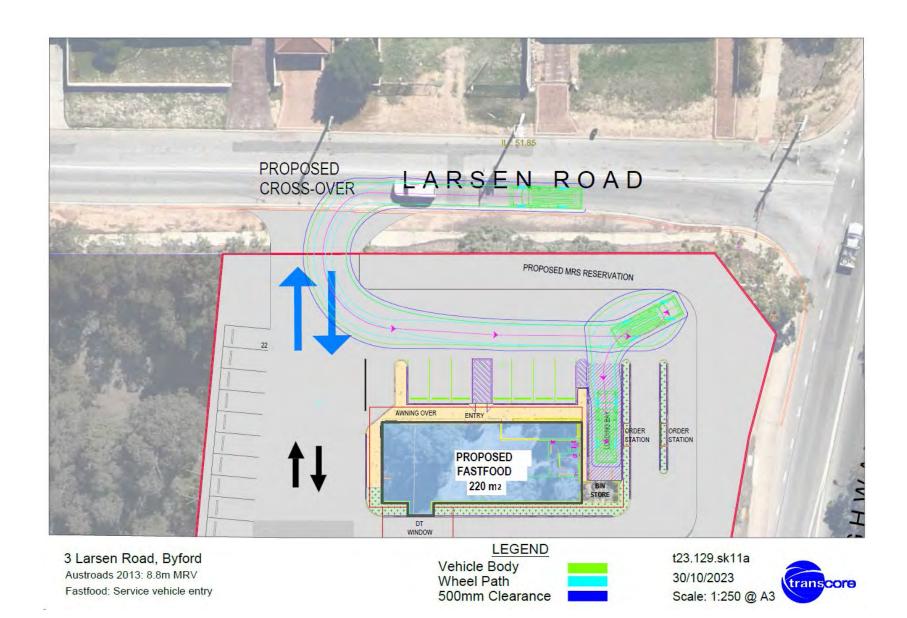
**TURN PATH ANALYSIS** 



Engineering a better future for over 20 years!











3 Larsen Road, Byford

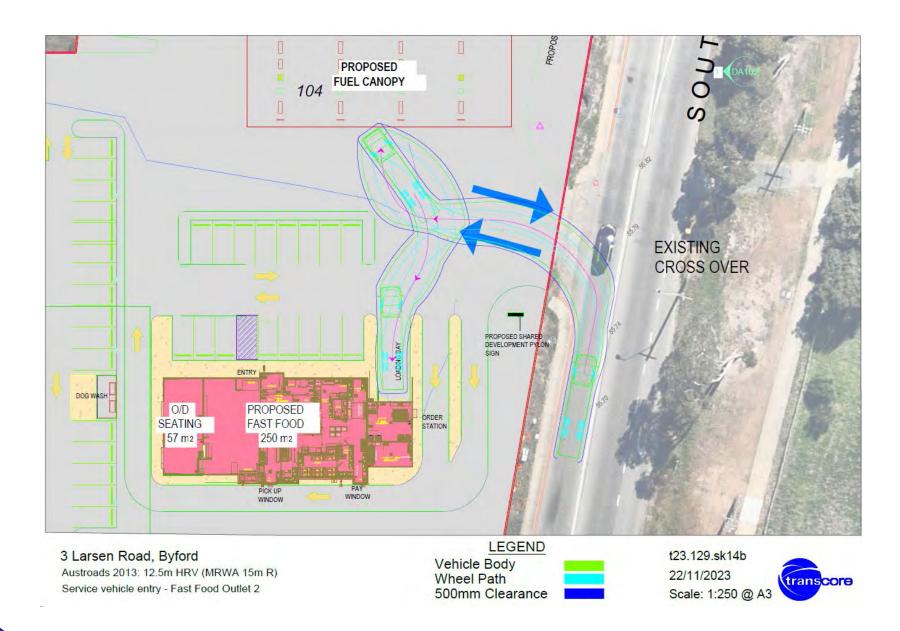
Austroads 2013: 12.5m HRV Service Station: Service vehicle entry

LEGEND Vehicle Body Wheel Path 500mm Clearance

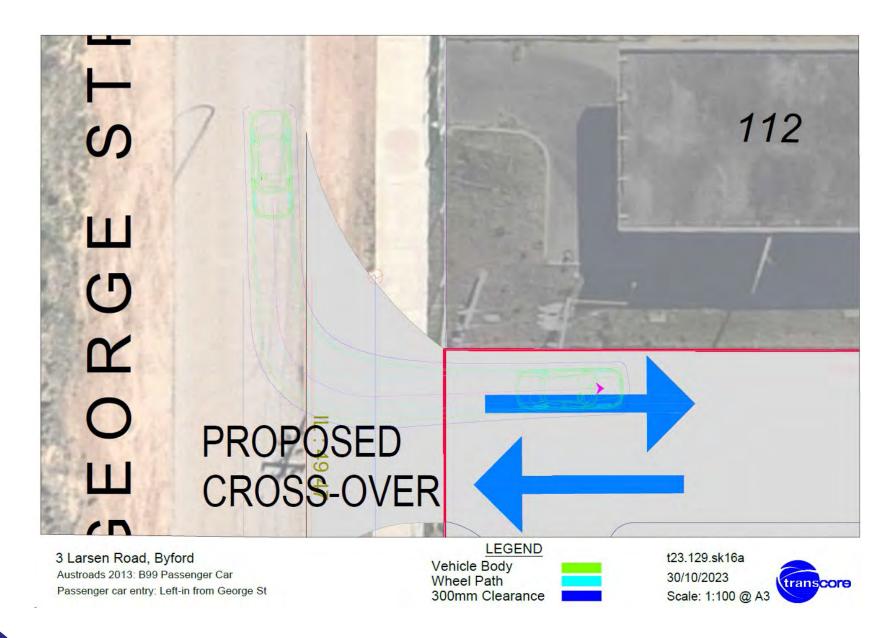
t23.129.sk13a 30/10/2023

Scale: 1:400 @ A3

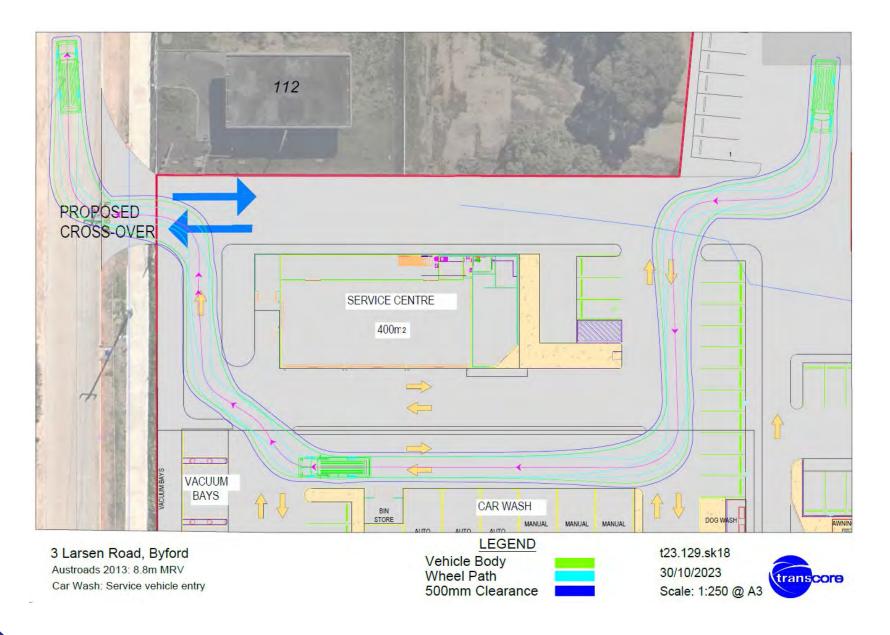












# **Appendix C**

**SIDRA RESULTS** 

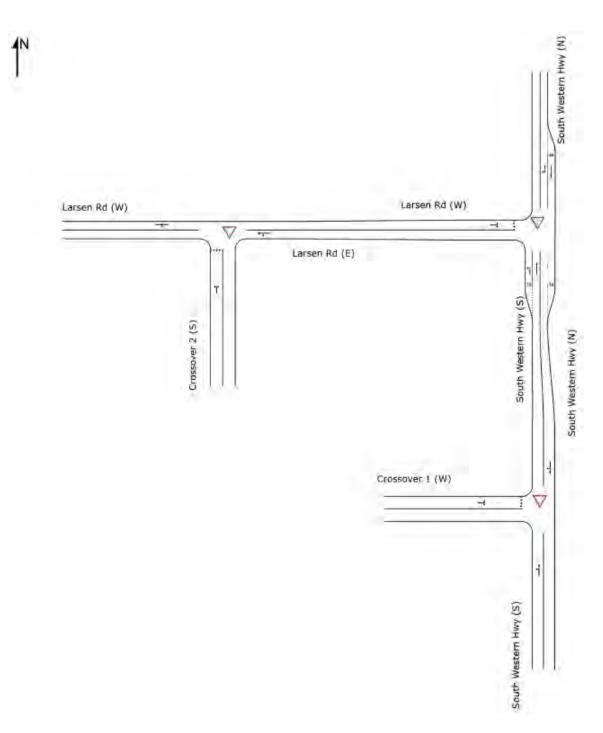


Figure C1: Network layout modelled in SIDRA

V Site: [South Western Hwy & Larsen Rd - Existing - AM (Site

Folder: Existing - Calibrated - 2021)]

Site Category: (None) Give-Way (Two-Way)

Mov	Tum	ovemen INP		DEM	AND	Deg.	Aune	Level of	05% P	ACK OF	Prop.	Effective	Aver	Aver
ID	Turn	VOLU [Total		FLO [Total		Satn		Service		EUE Dist]	Que	Stop Rate		Spee
		veh/h	%	veh/h	%	v/c	sec		veh	m		1000	20000	km/f
Sout	h: Sou	th Wester	n Hwy (	S)										
7	L2	86	4.1	91	4.1	0.052	5.6	LOSA	0.0	0.0	0.00	0.58	0.00	42.6
8	T1	747	7.9	786	7.9	0.449	0.1	LOSA	0.0	0.0	0.00	0.00	0.00	59.6
Appr	oach	833	7.5	877	7.5	0.449	0.6	NA	0.0	0.0	0.00	0.06	0.00	57.7
Nort	h: Sout	h Wester	n Hwy (I	N)										
2	T1	515	9.8	542	9.8	0.316	0.2	LOSA	0.0	0.0	0.00	0.00	0.00	59.8
3	R2	61	4.1	64	4.1	0.153	13.4	LOS B	0.5	4.1	0.74	0.89	0.74	35.4
Appr	roach	576	9.2	606	9.2	0.316	1.6	NA	0.5	4.1	0.08	0.09	0.08	55.7
Wes	t: Larse	en Rd (W	)											
4	L2	136	3.8	143	3.8	0.854	38.5	LOS E	5.8	44.5	0.94	1.52	2.66	19.2
6	R2	52	3.8	55	3.8	0.854	72.1	LOS F	5.8	44.5	0.94	1.52	2.66	16.0
Appr	oach	188	3.8	198	3.8	0.854	47.8	LOS E	5.8	44.5	0.94	1.52	2.66	18.4
All Vehi	cles	1597	7.7	1681	7.7	0.854	6.5	NA	5.8	44.5	0.14	0.24	0.34	46.0

#### MOVEMENT SUMMARY

∇ Site: [South Western Hwy & Larsen Rd - Existing - PM (Site)

Folder: Existing - Calibrated - 2021)]

Vehi	icle M	ovemen	t Perfo	rmance										
Mov ID	Tum	INP VOLU [Total		DEM FLC [Total		Deg. Satn		Level of Service		ACK OF EUE Dist]	Prop. Que	Effective Stop Rate	Aver. No. Cycles	Aver Speed
		veh/h	%	veh/h	%	v/c	sec		veh	m	_	27500	100	km/r
Sout	h: Sout	h Wester	m Hwy (	S)										
7	L2	149	4.1	157	4.1	0.090	5.6	LOSA	0.0	0.0	0.00	0.58	0.00	42.6
8	T1	579	7.9	609	7.9	0.348	0.0	LOSA	0.0	0.0	0.00	0.00	0.00	59.8
Appr	oach	728	7.1	766	7.1	0.348	1.2	NA	0.0	0.0	0.00	0.12	0.00	56.0
North	h: Sout	h Wester	n Hwy (l	N)										
2	T1	818	9.8	861	9.8	0.502	0.3	LOSA	0.0	0.0	0.00	0.00	0.00	59.5
3	R2	92	4.1	97	4.1	0.182	11.4	LOS B	0.7	5.2	0.67	0.87	0.67	37.2
Appr	oach	910	9.2	958	9.2	0.502	1.4	NA	0.7	5.2	0.07	0.09	0.07	56.
Wes	t: Larse	en Rd (W	)											
4	L2	67	3.8	71	3.8	0.783	35.0	LOS D	4.1	31.2	0.92	1.33	2.04	18.
6	R2	64	3.8	67	3.8	0.783	70.3	LOS F	4.1	31.2	0.92	1.33	2.04	15.0
Appr	oach	131	3.8	138	3.8	0.783	52.2	LOS F	4.1	31.2	0.92	1.33	2.04	16.
All Vehic	cles	1769	8.0	1862	8.0	0.783	5.1	NA	4.1	31.2	0.10	0.19	0.19	48.3



V Site: [South Western Hwy & Larsen Rd - 2025 - AM (Site

Folder: 2025 - With Development)]

■■ Network: N101 [AM (Network Folder: 2025 - With Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Veh	icle Mo	vement	Perfo	rmand	e					Level 1	100			
Mov ID	Tum	DEM/ FLO [Total veh/h	WS	ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c		Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
Sout	h: South	Wester	n Hwy (	S)										
7	L2	22	4.1	22	4.1	0.013	5,3	LOSA	0.0	0.0	0.00	0.57	0.00	31.8
8	T1	852	7.9	852	7.9	0.486	0.0	LOSA	0.0	0.0	0.00	0.00	0.00	59.6
Appr	roach	874	7.8	874	7.8	0.486	0.2	NA	0.0	0.0	0.00	0.01	0.00	59.2
Nort	h: South	Western	Hwy (	N)										
2	T1	577	9.8	577	9.8	0.336	0.2	LOSA	0.0	0.0	0.00	0.00	0.00	59.8
3	R2	51	4.1	51	4.1	0.126	13.6	LOS B	0.4	3.3	0.74	0.90	0.74	31.9
Appr	roach	627	9.3	627	9.3	0.336	1.2	NA	0.4	3.3	0.06	0.07	0.06	55.8
Wes	t: Larser	Rd (W)												
4	L2	56	3.8	56	3.8	0.596	24.1	LOS C	2.3	17.7	0.93	1.11	1.42	18.3
6	R2	40	3.8	40	3.8	0.596	58.7	LOSF	2.3	17.7	0.93	1.11	1.42	5.0
Appr	roach	96	3.8	96	3.8	0.596	38.5	LOSE	2.3	17.7	0.93	1.11	1.42	13.8
All V	ehicles	1597	8.2	1597	8.2	0.596	2.9	NA	2.3	17.7	0.08	0.10	0.11	51.2

#### MOVEMENT SUMMARY

V Site: [South Western Hwy & Crossover 1 - 2025 - AM (Site

Folder: 2025 - With Development)]

■■ Network: N101 [AM (Network Folder: 2025 - With Development - 2% pa growth)]

Vehi	icle Mo	vement	Perfo	rmano	e		-	10.00	1000	200		-		
Mov ID	Tum	DEM/ FLO [Total veh/h	WS	ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c	Aver. Delay sec	Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	lver. No. Cycles	Aver. Speed km/h
Sout	h: South	Western	n Hwy (	(S)										
7 8	L2 T1	36 855	2.0 7.9	36 855	2.0 7.9	0.471 0.471	5.8 0.2	LOS A	0.0	0.0	0.00	0.02 0.02	0.00	49.1 59.2
Appr	oach	891	7.7	891	7.7	0.471	0.4	NA	0.0	0.0	0.00	0.02	0.00	58.7
North	h: South	Western	Hwy (	N)										
2	T1 R2	613 4	9.8	613 4	9.8 2.0	0.339	0.2 15.2	LOS A	0.2 0.2	1.4	0.03	0.00	0.03	59.5 60.0
Appr	oach	617	9.7	617	9.7	0.339	0.3	NA	0.2	1.4	0.03	0.00	0.03	59.5
Wes	t: Cross	over 1 (V	V)											
4	L2	19	2.0	19	2.0	0.078	5.5	LOSA	0.2	1.8	0.79	0.79	0.79	7.2
6	R2	3	2.0	3	2.0	0.078	46.1	LOSE	0.2	1.8	0.79	0.79	0.79	38.3
Appr	oach	22	2.0	22	2.0	0.078	11.3	LOS B	0.2	1.8	0.79	0.79	0.79	17.2
All V	ehicles	1529	8.4	1529	8.4	0.471	0.5	NA	0.2	1.8	0.02	0.03	0.02	58.6

V Site: [Larsen Rd & Crossover 2 - 2025 - AM (Site Folder: 2025 - With Development)]

■■ Network: N101 [AM (Network Folder: 2025 - With Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehi	icle Mo	vement	Perfo	rmano	ce	-			1000	-6-				20.0
Mov ID	Tum	DEM/ FLO\ [Total veh/h		ARRI FLO [Total veh/h	WS IHV]	Deg. Satn v/c	Aver. Delay sec	Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver Speed km/h
Sout	h: Cross	over 2 (S	3)											
4	L2	7	2.0	7	2.0	0.060	0.1	LOSA	0.2	1.5	0.15	0.10	0.15	25.6
6	R2	64	2.0	64	2.0	0.060	0.6	LOSA	0.2	1.5	0.15	0.10	0.15	19.3
Appr	oach	72	2.0	72	2.0	0.060	0.5	LOSA	0.2	1.5	0.15	0.10	0.15	20.1
East	Larsen	Rd (E)												
7	L2	42	2.0	42	2.0	0.039	3.7	LOSA	0.0	0.0	0.00	0.31	0.00	39.6
8	T1	31	4.1	31	4.1	0.039	0.0	LOSA	0.0	0.0	0.00	0.31	0.00	41.7
Appr	oach	73	2.9	73	2.9	0.039	2.1	NA	0.0	0.0	0.00	0.31	0.00	40.4
West	t: Larser	Rd (W)												
2	T1	32	3.8	32	3.8	0.026	0.1	LOSA	0.1	0.6	0.11	0.18	0.11	39.4
3	R2	16	2.0	16	2.0	0.026	4.8	LOSA	0.1	0.6	0.11	0.18	0.11	29.3
Appr	oach	47	3.2	47	3.2	0.026	1.7	NA	0.1	0.6	0.11	0.18	0.11	33.6
All Ve	ehicles	192	2.6	192	2.6	0.060	1.4	NA	0.2	1.5	0.08	0.20	0.08	29.2

#### MOVEMENT SUMMARY

V Site: [South Western Hwy & Larsen Rd - 2025 - PM (Site Folder: 2025 - With Development)]

Polder: 2025 - With Development - 2% pa growth)]

Veh	icle Mo	vement	Perfo	rmano	e			-		and the same			000	
Mov ID	Tum	DEM/ FLO\ [Total veh/h		ARRI FLO [ Total veh/h	WS HV]	Deg. Satn v/c	Aver. Delay sec	Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	lver. No. Cycles	Aver. Speed km/h
Sout	h: South	Western	h Hwy	(S)										
7 8	L2 T1	36 660	4.1 7.9	36 660	4.1 7.9	0.020 0.377	5.4 0.0	LOS A	0.0	0.0	0.00	0.57 0.00	0.00	31.8 59.7
Appr	oach	696	7.7	696	7.7	0.377	0.3	NA	0.0	0.0	0.00	0.03	0.00	58.9
Nort	h: South	Western	Hwy (	N)										
2	T1	918	9.8	918	9.8	0.535	0.3	LOSA	0.0	0.0	0.00	0.00	0.00	59.5
3	R2	64	4.1	64	4.1	0.112	10.5	LOS B	0.4	3.1	0.62	0.85	0.62	35.7
Appr	roach	982	9.4	982	9.4	0.535	1.0	NA	0.4	3.1	0.04	0.06	0.04	57.0
Wes	t: Larser	n Rd (W)												
4	L2	44	3.8	44	3.8	0.593	21.6	LOS C	2.3	17.4	0.91	1.11	1.40	17.8
6	R2	48	3.8	48	3.8	0.593	57.2	LOSF	2.3	17.4	0.91	1.11	1.40	4.8
Appr	oach	93	3.8	93	3.8	0.593	40.2	LOSE	2.3	17.4	0.91	1.11	1.40	12.1
All V	ehicles	1771	8.5	1771	8.5	0.593	2.8	NA	2.3	17.4	0.07	0.10	0.10	51.5

V Site: [South Western Hwy & Crossover 1 - 2025 - PM (Site Folder: 2025 - With Development)]

■■ Network: N101 [PM (Network

Folder: 2025 - With

Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Veh	icle Mo	vement	Perfo	rmano	e	-	100	1000	1.4.2	224	-			
Mov ID	Tum	DEM/ FLO\ [Total veh/h	WS	ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c	Aver. Delay sec	Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
Sout	th: South	Western	Hwy (	(S)										
7	L2	42	2.0	42	2.0	0.377	5.7	LOSA	0.0	0.0	0.00	0.04	0.00	49.1
8	T1	672	7.9	672	7.9	0.377	0.1	LOSA	0.0	0.0	0.00	0.04	0.00	59.1
Appi	roach	714	7.6	714	7.6	0.377	0.5	NA	0.0	0.0	0.00	0.04	0.00	58.4
Nort	h: South	Western	Hwy (	N)										
2	T1	962	9.8	962	9.8	0.527	0.1	LOSA	0.2	1.7	0.02	0.00	0.03	59.7
3	R2	5	2.0	5	2.0	0.527	14.1	LOS B	0.2	1.7	0.02	0.00	0.03	60.8
Аррі	roach	967	9.8	967	9.8	0.527	0.2	NA	0.2	1.7	0.02	0.00	0.03	59.7
Wes	t: Cross	over 1 (V	V)											
4	L2	25	2.0	25	2.0	0.092	3.4	LOSA	0.3	2.1	0.73	0.70	0.73	8.0
6	R2	4	2.0	4	2.0	0.092	47.0	LOSE	0.3	2.1	0.73	0.70	0.73	39.7
Аррі	roach	29	2.0	29	2.0	0.092	9.6	LOS A	0.3	2.1	0.73	0.70	0.73	18.6
All V	ehicles	1711	8.7	1711	8.7	0.527	0.5	NA	0.3	2.1	0.02	0.03	0.03	58.7

#### MOVEMENT SUMMARY

V Site: [Larsen Rd & Crossover 2 - 2025 - PM (Site Folder: 2025 - Network: N101 [PM (Network Folder: 2025 - With - With Development)] Development - 2% pa growth)]

Vehi	cle Mo	vement	Perfo	rmano	e	100			100	100	W 11 1			
Mov ID	Tum	DEM/ FLO/ [Total veh/h		ARRI FLO [Total veh/h	WS IHV]	Deg. Satn		Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver Speed km/h
South	n: Cross	sover 2 (S	3)											
4	L2	8	2.0	8	2.0	0.071	0.2	LOSA	0.2	1.8	0.18	0.12	0.18	25.5
6	R2	76	2.0	76	2.0	0.071	0.6	LOSA	0.2	1.8	0.18	0.12	0.18	19.2
Appro	oach	84	2.0	84	2.0	0.071	0.6	LOSA	0.2	1.8	0.18	0.12	0.18	20.0
East:	Larsen	Rd (E)												
7	L2	49	2.0	49	2.0	0.054	3.7	LOSA	0.0	0.0	0.00	0.26	0.00	40.4
8	T1	51	4.1	51	4.1	0.054	0.0	LOSA	0.0	0.0	0.00	0.26	0.00	42.7
Appro	oach	100	3.1	100	3.1	0.054	1.8	NA	0.0	0.0	0.00	0.26	0.00	41.5
West	: Larser	Rd (W)												
2	T1	17	3.8	17	3.8	0.021	0.2	LOSA	0.1	0.7	0.18	0.27	0.18	35.1
3	R2	19	2.0	19	2.0	0.021	4.9	LOSA	0.1	0.7	0.18	0.27	0.18	28.0
Appro	oach	36	2.8	36	2.8	0.021	2.7	NA	0.1	0.7	0.18	0.27	0.18	29.8
All Ve	ehicles	220	2.6	220	2.6	0.071	1.5	NA	0.2	1.8	0.10	0.21	0.10	29.1



#### **Engineering a better future for over 20 years!**

**Technical Note:** No 2a **Date:** 20/03/2024

Project No: t23.129

Project: Lot 104 (No 3) Larsen Road, Byford

Subject: Assessment of the revised access arrangement for the development and

addressing Main Roads WA comments

#### 1 Introduction

This technical note has been prepared by Transcore on behalf of Capital Prudential with respect to the revised access arrangement for the proposed new development entailing Service Station, Fast Food Outlet, Motor Vehicle Repair and Motor Vehicle Wash land uses at the abovementioned site.

This technical note is an addendum to the Transport Impact Assessment (TIA) report prepared by Transcore in November 2023 and will address the removal of the George Street crossover and recent Main Roads WA comments outlined in their letter of 14 Match 2024 with respect to:

- SIDRA analysis of the left in crossover on South Western Highway (SWH); and,
- Lack of physical restriction at the SWH crossover to enforce left in movement.

The SIDRA analysis for the left in only crossover on South Western Highway has been undertaken and the SIDRA files has been provided to Main Roads.

The Applicant's proposal for the left-in only movement at the existing SWH crossover is to enforce it through signage and line markings without any physical modifications. However, if Main Roads WA supports the proposed left-in only crossover on SWH, the Applicant is prepared to accept a suitably worded development approval condition to design the crossover in a way that it physically enforces the left-in only movements.

The Public Transport Authority's referral comment regarding the connection to George Street has been addressed in the updated plan by removing this development crossover on George Street. A copy of the updated development site plan, reflecting this change, is provided in **Appendix A**. Additionally, the turn paths for the fuel tanker has been updated to reflect this modification, and the turn path plans are provided in **Appendix B**.

As a result of the removal of the George Street crossover, the development trip distribution and SIDRA analysis have been updated to reflect this change.

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www.transcore.net.au www.linkedin.com/company/transcore/ instagram: @transcoreaustralia This technical note documents the outcome of the updated modelling and analysis for the updated development plan.

#### 2 Assessment Period

The assessment year that is adopted for the analysis is 2025. It is anticipated that the construction of Byford Station will take place in the near future, resulting in a decrease in the car mode share within the immediate vicinity. This change, coupled with the introduction of a new park and ride facility, may alter the traffic patterns in the area.

Additionally, the recently announced and funded Tonkin Highway extension project is expected to divert regional traffic away from SWH, leading to a reduction in existing traffic volumes after the completion of the extension, which is anticipated in the short term. On this basis the assessment undertaken does not include 10 years post development scenario.

### 3 Trip generation and distribution

The proposed removal of the George Street crossover would not change the trip generation of the proposed development; however, the trip distribution of the development would change and the turning movements at the George Street crossover would be shifted to the Larsen Road crossover.

The updated distribution of the proposed development traffic is illustrated in **Figure**1 for the AM and PM peak hours.

The proposed relocation of the railway level crossing from Larsen Road further south to Clara Street would remove most of the existing traffic along Larsen Road towards SWH. Accordingly, the redistributed traffic on the surrounding road network in 2025 after closure of the railway crossing was estimated and the development traffic was added to the redistributed traffic. A 2% per year traffic growth rate was applied to the background traffic to establish the 2025 traffic on SWH and George Street.

The total projected traffic volumes for the assessment year are presented in **Figure 2**.

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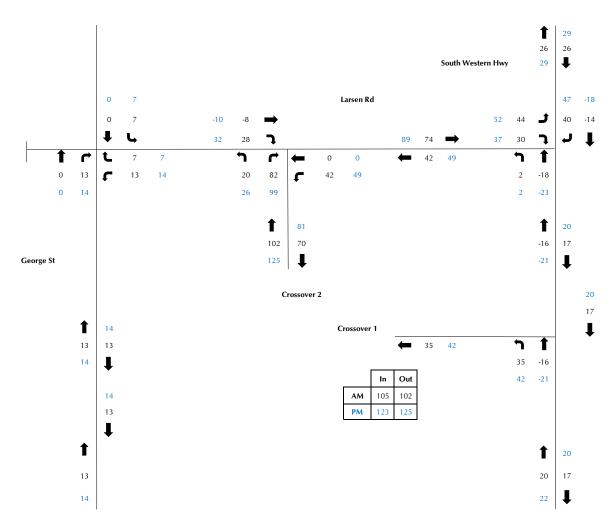


Figure 1: Updated development trip distribution during the AM and PM peak hours

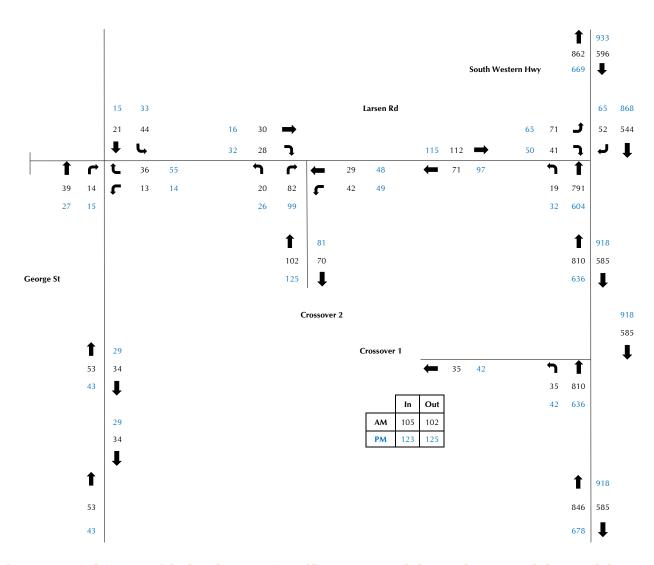


Figure 2: Total (2025 with development) traffic - AM Weekday and PM Weekday peak hours

#### 4 SIDRA Results

Capacity analysis of the development crossovers on Larsen Road and SWH and intersection of Larson Road/SWH was undertaken using the SIDRA computer software package.

The results of the SIDRA analysis are summarised in Appendix C. The SIDRA intersection models were coded with reference to Main Roads WA Operation Modelling Guidelines. All relevant parameters such as heavy vehicle groups, PCU factors etc. were coded as per the Main Roads WA Guidelines.

#### **SWH/Larsen Road intersection**

The SIDRA analysis results and site observations indicate that the intersection of SWH/ Larsen Road presently operates at capacity with level of service F for the critical right turn movement out of Larsen Road during both weekday peak hours. The gap acceptance and follow up parameters in SIDRA were adjusted slightly for this movement to calibrate to the 2021 queues and delays at the intersection. Table 1 summarises the calibrated queues and delays at the intersection for the critical right turn movements out of Larsen Road.

Table 1: SIDRA results for the critical right turn movements at the SWH / **Larsen Rd intersection in 2021** 

	Moveme	nt: Right t	urn out from	Larsen Rd
	Observe	d (2021)	Modelle	d (2021)
	AM	PM	AM	PM
95% back of queue (Veh)	5.3	4.6	5.8	4.1
Average delay time (S)	68	52	72.1	70.3
LoS	F	F	F	F

The closure of the railway crossing at Larsen Road and the addition of the development-generated traffic to the intersection will result in less traffic at the intersection in 2025 compared to 2021 and consequently minor decreases in overall queues and delays are reported. No change in overall LoS for the intersection is reported. Table 2 summarises the performance parameters for the critical right turn movements out of Larsen Road in 2025.

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Table 2: SIDRA results for the critical right movements at the SWH / Larsen Rd intersection in 2025

	Movement: Right tur	n out from Larsen Rd
	2025 After road closure	and with development
	AM	PM
95% back of queue (Veh)	2.7	2.8
Average delay time (S)	57.9	56.7
LoS	F	F

#### SWH left in crossover

SIDRA analysis indicates that the proposed left in crossover on SWH will operate satisfactorily in 2025 with LoS A and minimal queues and delays during assessed peak hours.

#### **Larsen Road crossover**

SIDRA analysis indicates that the proposed development crossover on Larson Road will operate satisfactorily in 2025 during assessed peak hours. All movements operate with acceptable levels of service with minimal delays and queuing.

#### **Network Operations**

Relevant SIDRA network outputs were reviewed for assessed peak hours to establish the operation of the SWH/ Larsen Road intersection and development crossovers on Larsen Road and SWH as an integrated network.

As detailed in **Figure 3** there are no queue backs reported from the SWH/ Larsen Road intersection to the proposed development crossovers on Larsen Road and SWH. Similarly, no queue backs from the development crossover on Larsen Road to SWH intersection is reported.

Hence, the capacity analysis confirms that the proposed development with the revised crossover arrangement will not have an adverse impact on the operation of the road network and that the proposed development crossovers on Larsen Road and SWH will operate satisfactorily.

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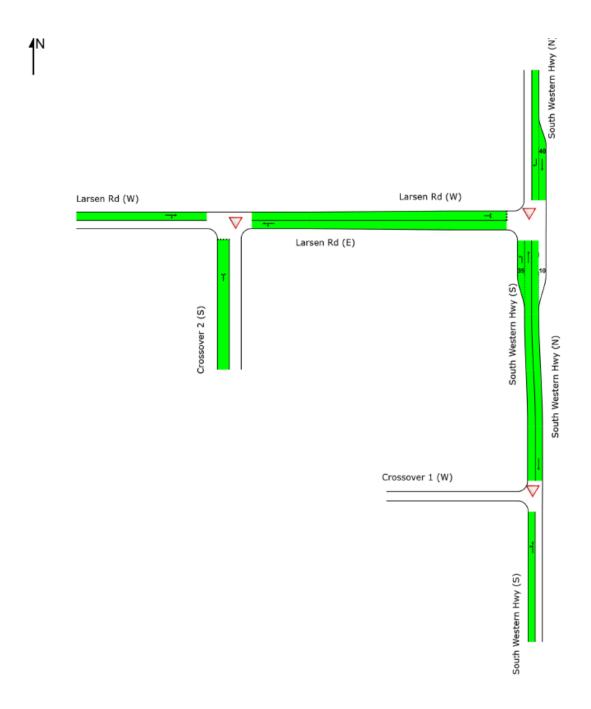


Figure 3: Critical weekday AM/PM peak hour network analysis – queue storage ratio (2025)

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Ordrinary Council Meeting - 20 May 202

# 5 Conclusion

In response to Main Roads WA's concern regarding the SWH crossover, the proposed development now only entails a left in only crossover on South Western Highway.

The Applicant's proposes that the left-in only movements at the existing SWH crossover is enforced through signage and line markings without any physical modifications. However, if Main Roads WA supports the proposed left-in only crossover on SWH, the Applicant is prepared to accept a suitably worded development approval condition to design the crossover in a way that it physically enforces the left-in only movements.

In response to Public Transport Authority (PTA) referral comments regarding the connection to George Street, the proposed development George Street crossover is removed in the updated development plan. Turn paths undertaken for the fuel tanker shows the tanker can satisfactorily enter and exit the site without reliance on George Street crossover.

The assessment year that is adopted for the analysis is 2025. It is anticipated that the construction of Byford Station will result in a decrease in the car mode share within the immediate vicinity. Additionally, the recently announced and funded Tonkin Highway extension project is expected to divert regional traffic away from South Western Highway, leading to a reduction in existing traffic volumes in the short term.

The closure of the railway crossing at Larsen Road and the addition of the development-generated traffic to the intersection is estimated to result in less traffic at the intersection in 2025 (post development) compared to existing situation and consequently minor decreases in overall queues and delays are reported by SIDRA.

It is concluded that downgrading the existing SWH crossover to left in only and removal of the George Street crossover would not adversely impact the traffic operation of the intersection of SWH/ Larsen Road and the development Larson Road crossover.

SIDRA analysis indicates that the proposed left in only crossover on SWH will operate satisfactorily in 2025 with LOS A and minimal queues and delays during assessed peak hours.

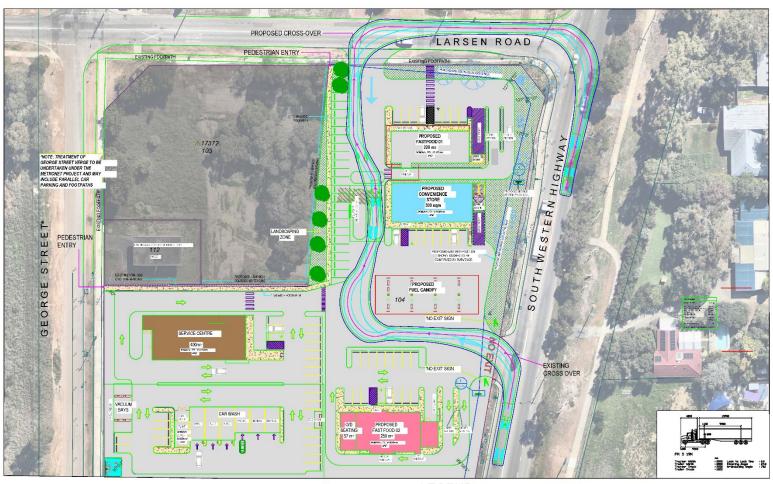
# **APPENDIX A**

# PROPOSED REVISED DEVELOPMENT SITE PLAN



# **APPENDIX B**

# **TURN PATHS**



3 Larsen Road, Byford Austroads 2013: 19.0m Fuel-tanker (MRWA 15m R) Fuel-tanker circulation LEGEND
Vehicle Body
Wheel Path
500mm Clearance

t23.129.sk21 20/03/2024 Scale: 1:600 @ A3



# **APPENDIX C**

# **SIDRA RESULTS**

### **MOVEMENT SUMMARY**

V Site: [Larsen Rd & Crossover 2 - 2025 - AM (Site Folder: 2025 **■■ Network: N101 [AM** - With Development)] (Network Folder: 2025 - With Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehi	cle Mo	vement	Perfo	rmano	e									
Mov ID	Tum	DEMA FLOV [Total veh/h		ARRI FLO [Total veh/h	WS IHV]	Deg. Satn v/c		Level of Service		ACK OF IEUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	h: Cross	sover 2 (S	6)											
4	L2	21	2.0	21	2.0	0.089	0.1	LOSA	0.3	2.3	0.14	0.10	0.14	25.7
6	R2	86	2.0	86	2.0	0.089	0.6	LOS A	0.3	2.3	0.14	0.10	0.14	19.3
Appr	oach	107	2.0	107	2.0	0.089	0.5	LOSA	0.3	2.3	0.14	0.10	0.14	20.9
East:	Larsen	Rd (E)												
7	L2	44	2.0	44	2.0	0.040	3.7	LOS A	0.0	0.0	0.00	0.31	0.00	39.4
8	T1	31	4.1	31	4.1	0.040	0.0	LOSA	0.0	0.0	0.00	0.31	0.00	41.5
Appr	oach	75	2.9	75	2.9	0.040	2.2	NA	0.0	0.0	0.00	0.31	0.00	40.2
West	: Larser	n Rd (W)												
2	T1	32	3.8	32	3.8	0.035	0.2	LOS A	0.1	1.1	0.15	0.25	0.15	36.2
3	R2	29	2.0	29	2.0	0.035	4.8	LOS A	0.1	1.1	0.15	0.25	0.15	28.3
Appr	oach	61	2.9	61	2.9	0.035	2.4	NA	0.1	1.1	0.15	0.25	0.15	30.7
All Ve	ehicles	243	2.5	243	2.5	0.089	1.5	NA	0.3	2.3	0.10	0.20	0.10	27.6

### **MOVEMENT SUMMARY**

V Site: [South Western Hwy & Crossover 1- 2025 - AM (Site

Folder: 2025 - With Development)]

■ Network: N101 [AM (Network Folder: 2025 - With

Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehi	cle Mo	vement	Perfo	rmanc	:e									
Mov ID	Tum	DEMA FLON [Total veh/h	NS	ARRI FLO' [Total veh/h	WS HV]	Deg. Satn v/c		Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	n: South	Westerr	Hwy (	S)										
7	L2	37	2.0	37	2.0	0.508	5.8	LOS A	0.0	0.0	0.00	0.02	0.00	48.4
8	T1	853	7.9	853	7.9	0.508	0.2	LOS A	0.0	0.0	0.00	0.02	0.00	59.1
Appro	oach	889	7.7	889	7.7	0.508	0.5	NA	0.0	0.0	0.00	0.02	0.00	58.5
North	: South	Western	Hwy (	N)										
2	T1	616	9.8	616	9.8	0.359	0.0	LOS A	0.0	0.0	0.00	0.00	0.00	59.7
Appro	oach	616	9.8	616	9.8	0.359	0.0	NA	0.0	0.0	0.00	0.00	0.00	59.7
All Ve	ehicles	1505	8.5	1505	8.5	0.508	0.3	NA	0.0	0.0	0.00	0.01	0.00	59.0

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### MOVEMENT SUMMARY

▽ Site: [South Western Hwy & Larsen Rd - 2025 - AM (Site

Folder: 2025 - With Development)]

Network: N101 [AM (Network Folder: 2025 - With Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehic	cle Mo	vement	Perfo	rmano	e									
Mov ID	Tum	DEMA FLOV [Total veh/h	NS	ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c		Level of Service		ACK OF JEUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	: South	Western	Hwy (	(S)										
7 8	L2 T1	20 833	4.1 7.9	20 833	4.1 7.9	0.011 0.475	5.3 0.0	LOS A LOS A	0.0 0.0	0.0 0.0	0.00	0.57 0.00	0.00	31.8 59.6
Appro	ach	853	7.8	853	7.8	0.475	0.2	NA	0.0	0.0	0.00	0.01	0.00	59.2
North	: South	Western	Hwy (	N)										
2	T1 R2	573 55	9.8 4.1	573 55	9.8 4.1	0.334 0.131	0.2 13.2	LOS A LOS B	0.0 0.4	0.0 3.4	0.00 0.73	0.00 0.89	0.00 0.73	59.8 32.3
Appro	ach	627	9.3	627	9.3	0.334	1.3	NA	0.4	3.4	0.06	0.08	0.06	55.6
West:	Larser	Rd (W)												
4	L2	75	3.8	75	3.8	0.645	24.5	LOS C	2.7	20.8	0.92	1.15	1.54	18.9
6	R2	43	3.8	43	3.8	0.645	57.9	LOS F	2.7	20.8	0.92	1.15	1.54	5.3
Appro	ach	118	3.8	118	3.8	0.645	36.7	LOSE	2.7	20.8	0.92	1.15	1.54	14.9
All Ve	hicles	1598	8.1	1598	8.1	0.645	3.3	NA	2.7	20.8	0.09	0.12	0.14	50.1

### MOVEMENT SUMMARY

▼ Site: [Larsen Rd & Crossover 2 - 2025 - PM (Site Folder: 2025 ■ Network: N101 [PM (Network - With Development)] Folder: 2025 - With

Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehic	cle Mo	vement	Perfo	rmano	e									
Mov ID	Tum	DEMA FLOV [Total veh/h		ARRI FLO [Total veh/h	WS IHV]	Deg. Satn v/c		Level of Service		BACK OF UEUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	: Cross	over 2 (S	5)											
4	L2	27	2.0	27	2.0	0.110	0.2	LOSA	0.4	2.9	0.18	0.12	0.18	25.6
6	R2	104	2.0	104	2.0	0.110	0.7	LOSA	0.4	2.9	0.18	0.12	0.18	19.2
Appro	ach	132	2.0	132	2.0	0.110	0.6	LOSA	0.4	2.9	0.18	0.12	0.18	20.8
East:	Larsen	Rd (E)												
7	L2	52	2.0	52	2.0	0.055	3.7	LOSA	0.0	0.0	0.00	0.27	0.00	40.3
8	T1	51	4.1	51	4.1	0.055	0.0	LOSA	0.0	0.0	0.00	0.27	0.00	42.6
Appro	ach	102	3.0	102	3.0	0.055	1.9	NA	0.0	0.0	0.00	0.27	0.00	41.4
West:	Larser	Rd (W)												
2	T1	17	3.8	17	3.8	0.030	0.3	LOSA	0.1	1.0	0.20	0.34	0.20	32.9
3	R2	34	2.0	34	2.0	0.030	4.9	LOS A	0.1	1.0	0.20	0.34	0.20	27.3
Appro	ach	51	2.6	51	2.6	0.030	3.3	NA	0.1	1.0	0.20	0.34	0.20	28.2
All Ve	hicles	284	2.5	284	2.5	0.110	1.5	NA	0.4	2.9	0.12	0.21	0.12	27.5

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### MOVEMENT SUMMARY

∇ Site: [South Western Hwy & Crossover 1- 2025 - PM (Site Folder: 2025 - With Development)]

■■ Network: N101 [PM (Network Folder: 2025 - With Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehi	cle Mo	vement	Perfo	rmano	:e									
Mov ID	Tum	DEMA FLOV [Total veh/h		ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c		Level of Service		ACK OF EUE Dist] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	n: South	Western	Hwy (	S)										
7	L2	44	2.0	44	2.0	0.407	5.7	LOS A	0.0	0.0	0.00	0.04	0.00	48.4
8	T1	669	7.9	669	7.9	0.407	0.2	LOS A	0.0	0.0	0.00	0.04	0.00	59.0
Appro	oach	714	7.5	714	7.5	0.407	0.5	NA	0.0	0.0	0.00	0.04	0.00	58.1
North	: South	Western	Hwy (	N)										
2	T1	966	9.8	966	9.8	0.563	0.1	LOS A	0.0	0.0	0.00	0.00	0.00	59.4
Appro	oach	966	9.8	966	9.8	0.563	0.1	NA	0.0	0.0	0.00	0.00	0.00	59.4
All Ve	hicles	1680	8.8	1680	8.8	0.563	0.2	NA	0.0	0.0	0.00	0.02	0.00	58.9

### **MOVEMENT SUMMARY**

Site: [South Western Hwy & Larsen Rd - 2025 - PM (Site

Folder: 2025 - With Development)]

■■ Network: N101 [PM (Network Folder: 2025 - With

Development - 2% pa growth)]

Site Category: (None) Give-Way (Two-Way)

Vehic	le Mo	vement	Perfo	rmano	e									
Mov ID	Tum	DEMA FLOV [Total veh/h		ARRI FLO [Total veh/h	WS HV]	Deg. Satn v/c		Level of Service		ACK OF JEUE Dist ] m	Prop. Que	Effective A Stop Rate	ver. No. Cycles	Aver. Speed km/h
South	: South	Western	Hwy (	(S)										
7	L2	34	4.1	34	4.1	0.019	5.4	LOSA	0.0	0.0	0.00	0.57	0.00	31.8
8	T1	636	7.9	636	7.9	0.363	0.0	LOSA	0.0	0.0	0.00	0.00	0.00	59.7
Appro	ach	669	7.7	669	7.7	0.363	0.3	NA	0.0	0.0	0.00	0.03	0.00	58.9
North:	South	Western	Hwy (	N)										
2	T1	914	9.8	914	9.8	0.533	0.3	LOSA	0.0	0.0	0.00	0.00	0.00	59.5
3	R2	68	4.1	68	4.1	0.114	10.2	LOS B	0.4	3.2	0.60	0.84	0.60	36.2
Appro	ach	982	9.4	982	9.4	0.533	1.0	NA	0.4	3.2	0.04	0.06	0.04	56.9
West:	Larser	Rd (W)												
4	L2	68	3.8	68	3.8	0.646	21.8	LOS C	2.8	21.3	0.90	1.16	1.54	18.8
6	R2	53	3.8	53	3.8	0.646	56.7	LOS F	2.8	21.3	0.90	1.16	1.54	5.2
Appro	ach	121	3.8	121	3.8	0.646	37.0	LOS E	2.8	21.3	0.90	1.16	1.54	14.0
All Ve	hicles	1773	8.4	1773	8.4	0.646	3.2	NA	2.8	21.3	0.08	0.12	0.13	50.2



#### Engineering a better future for over 20 years!

**Technical Note:** No 1 **Date:** 18/02/2024

Project No: t23.129

Project: Lot 104 (No 3) Larsen Road, Byford

**Subject**: Addressing the Shire of Stephanite Jarrahdale comments

# 1 Introduction

This technical note has been prepared by Transcore on behalf of Capital Prudential with respect to the proposed new development entailing Service Station, Fast Food Outlet, Motor Vehicle Repair and Motor Vehicle Wash land uses at the abovementioned site.

Following consideration of the Development Application by the Shire, the Shire has provided the following comments on the Transport Impact Assessment prepared by Transcore (TIA dated November 2023):

- 1. Traffic Impact Assessment to be updated to show parking/demand assessment.
- 2. Assessment of turn treatment warrants for access and advice on the slip lane/road upgrade requirements.
- 3. Liaise with Metronet to show the most updated design of George St and design the access accordingly. Ensure swept path of 19m truck exiting to George St complies to Austroads and AS2890.1,

With respect to Item 3 the most recent advice received from Metronet states that "Metronet are still finalising design details for the design of George Street and will have a firmer layout of the final design in mid to late March. When this information is available, we will be happy to share it with you". Therefore Item 3 will be addressed when most updated design of George St becomes available.

Accordingly, this technical note will address Items 1 and 2. Copy of the latest development plan is included in **Appendix A**.

# 2 Parking requirement and supply

The parking requirement for the proposed development is established in line with LPS3 and is summarised in **Table 1**. This table also includes the parking supply associated with the development and the theoretical parking shortfall in accordance with LPS3.

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Transcore Pty Ltd ACN 094 951 318 ABN 19 094 951 318

**Table 1: Car parking assessment** 

Use	Requirement	Calculation	Bays Required
Fast Food Outlet 1	1 bay per 4 m <sup>2</sup> of counter and/or dining areas, 1 bay per 4 m <sup>2</sup> of public assembly areas and 1 bay per employee. Where a drive through facility is provided, 4 stacking bays and 1 waiting bay shall be provided	50m2 counter and dining areas,10 staff members, 4 stacking bays and Waiting Bay provided	22
Fast Food Outlet 2	1 bay per 4 m <sup>2</sup> of counter and/or dining areas, 1 bay per 4 m <sup>2</sup> of public assembly areas and 1 bay per employee. Where a drive through facility is provided, 4 stacking bays and 1 waiting bay shall be provided	100m2 counter and dining areas,10 staff members, 4 stacking bays and Waiting Bay provided	35
Motor Vehicle Repair	1 bay per 50 m <sup>2</sup> NLA and 1 bay per employee	400m2 NLA = 8 bays 8 employees = 8 bays	16
Motor Vehicle Wash	1 bay per 50 m <sup>2</sup> NLA and 1 bay per employee	220m NLA = 5 bays 0 employees = 0 bays	5
Service Station	2 bays per service bay and 1 bay per employee	3 employee	3
Total parking bays required			81
Total parking bays provided - On site			78
Total parking bays			78
Surplus (+)/ Shortfall (-)			-3

As evident based on LPS3, there would be a theoretical parking shortfall of only 3 bays for the proposed development. However, parking requirement calculation in accordance with LPS3 is simply establishes the sum of the parking requirement for each land use. This approach does not allow for the fact that patrons to the development may visit more than one land use and the fact that the peak operating times for each land use may be different.

For example, motor vehicle repair will be closed during peak times of the fast-food outlets.

In order to establish a more realistic parking requirement and demand for the proposed development, a temporal parking assessment was undertaken for the proposed development based on the anticipated peak operating times for each land use and the anticipated parking demand during other times. This assessment was undertaken for a typical Friday and typical Saturday when the peak parking demand for the proposed development is expected to occur. The assessments are provided in Section 3 of the technical note.

# 3 Parking Assessment

As the peak parking demand periods for the various land-uses within the proposed development does not completely overlap, a daily anticipated parking demand profile (for a typical Friday and a typical Saturday) was established for each of the proposed land-uses to estimate the anticipated actual combined parking demand throughout the day.

The percentage of parking demand assumptions outlined in **Table B1** and **Table B2** in **Appendix B** are based on the project team experience and operator's advice.

The anticipated demand for parking is then calculated by multiplying the anticipated percentage of parking demand for each land-use by its theoretical parking requirement in accordance with LPS3. The resulting estimated parking demands are summarised in **Table B3** (for a typical Friday) and **Table B4** (for a typical Saturday). The parking surplus (+)/ shortfall (-) for each land-use is calculated by subtracting the total anticipated parking demand from the proposed number of bays.

As shown in Figure 1, the maximum combined parking demand for a typical Friday is anticipated to occur at 13:00 and 14:00. During this period, it is estimated that a total of 9 bays would be unoccupied/available. Similarly, As detailed in Table B4 and Figure 2, the maximum combined parking demand for a typical Saturday is anticipated to occur at 12:00 and 19:00. During this period, it is estimated that a total of 18 bays would be unoccupied/available.

It should be noted the temporal parking assessment undertaken does not allow for cross trades between various land uses. Arguably the estimated parking demand will be less than that established in this assessment.

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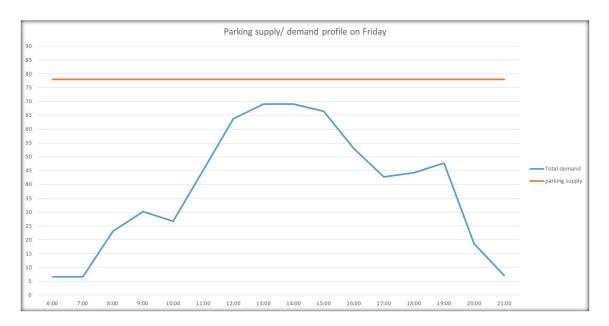


Figure 1: Parking supply/ demand on a typical Friday

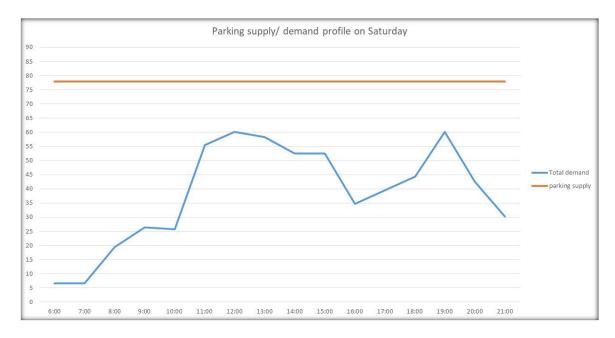


Figure 2: Parking supply/ demand on a typical Saturday

### 3.1 Turn Lane Assessment

Austroads Guide to Road Design Part 4A: Unsignalised and Signalised Intersections (2009) introduced new warrants for turn treatments on high-speed roads (>100km/h operating speed) and on low and intermediate speed roads (<100km/h operating speed), with graphs on page 45 presenting those warrants in terms of turning traffic volume against the opposing major road traffic volume (vehicles per hour).

t23.129.mr.tn01.docx Page 4 However, the warrants only distinguish between roads as having speeds above or below 100km/h. It is evident that accident frequency and severity are more likely to be greater at higher speeds, so there is some concern that relying on these warrants (above or below 100km/h) is very likely to over-prescribe the construction of costly turn treatments like channelised right turn lanes and left turn slip lanes (because of road widening required) on lower speed urban roads (eg. 60km/h speed limit on this section of South Western Highway).

In line with the Austroads Guide, Main Roads WA has prepared an excel spreadsheet for turn lane assessments, which has been utilised for the proposed development crossover on South Western Highway. The outcomes of the turn lane assessments for the AM and PM peak hours are presented in Appendix B, indicating that a right turn and left turn lane may be necessary at the crossover to meet Austroads requirements. It should be noted that the calculation of turn lane requirements is highly sensitive to the specific turning movements. For example, during the PM peak hour, there is an anticipated total of 5 right turn movements from South Western Highway to the development, resulting in a requirement for a channelised right turn lane (CHR). However, reducing the right turn movements to 4 would lead to a requirement for a basic auxiliary right turn lane (BAR), which is already in place at the crossover. It is also evident that the threshold for turn lane requirement is set very low and as a result turn lane treatments are not generally provided in low-speed urban environments due to significant costs and potential land impacts.

Accordingly, it is important to note that none of the existing crossovers on South Western Highway in the vicinity currently include turn lanes.

Main Roads WA has advised that this section of South Western Highway is planned for future upgrading, which will involve the provision of a median and extension of the existing left turn lane on South Western Highway to Larsen Road (refer Figure 3). Furthermore, due to the recently announced funded Tonkin High way extension project, any upgrade to South Western Highway is expected to be a long-term undertaking because the existing traffic volumes on South Western Highway will be reduced because at least the regional traffic will be diverted to Tonkin Highway.

Based on these considerations, it is recommended that the existing development crossover on South Western Highway should be retained in its current format until the upgrades to this section of the highway are implemented. Once the upgrades are finalised and put into effect, the existing crossover on South Western Highway may be downgraded to a left in/left out crossover because of the centre median. It should be also noted that there are numerous examples where Main Roads has upgraded its roads while maintaining a crossover within a new left turn lane as part of an upgraded intersection (e.g., Albany Hwy, Great Eastern Hwy, etc.).

It is also important to note that the retention of the development crossover on South Western Highway is critical to reduce the traffic demand at the intersection of South Western Highway and Larson Road.

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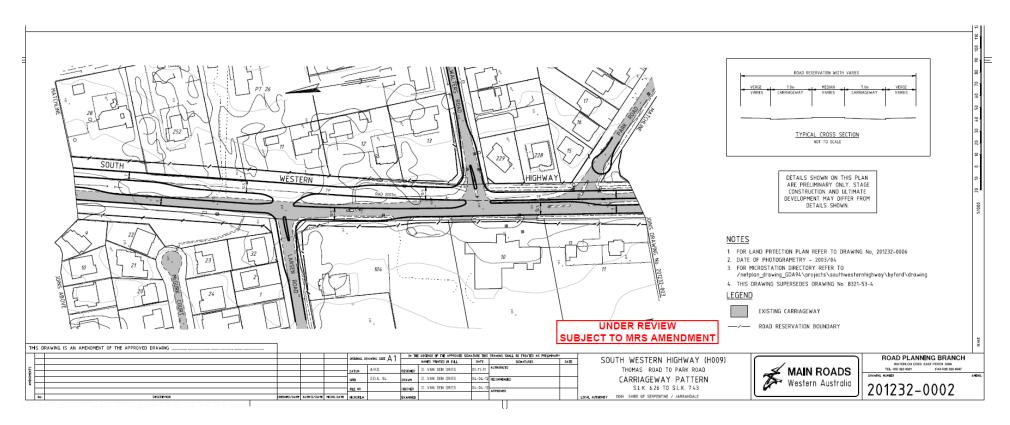


Figure 3: Proposed future upgrades on South Western Highway in the vicinity of the subject site

# 5 Conclusion

The parking investigations and assessments undertaken and documented in this technical note indicates that the parking provision of the proposed development meets and exceeds the anticipated actual typical peak parking demand of the development.

Considering the low operating speed on this section of South Western Highway and the absence of turn lanes at existing crossovers in the vicinity (low speed urban environment), it is determined that turn lanes are not necessary at the development crossover, particularly considering the significant costs and potential land impacts.

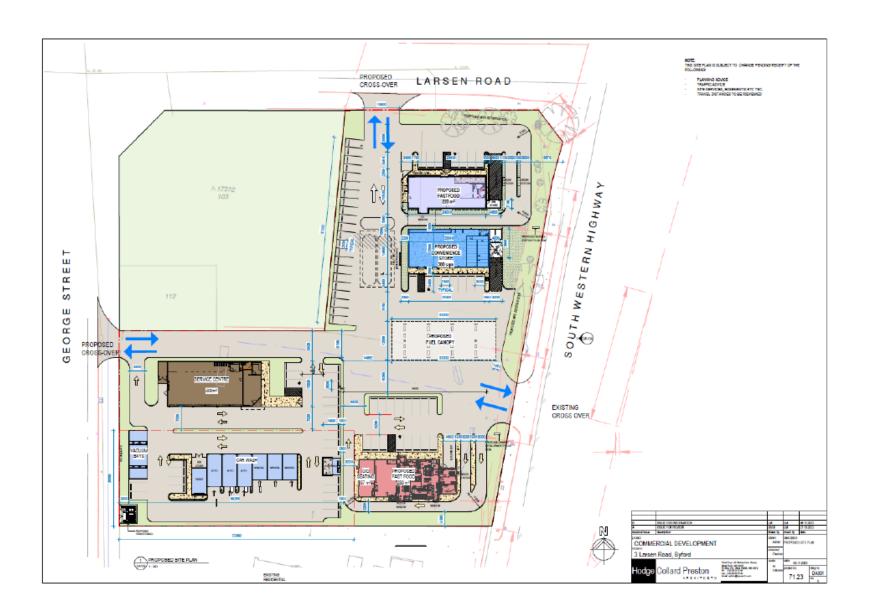
Main Roads WA has provided advice indicating that future upgrades to this section of South Western Highway will include the introduction of a median and an extension of the existing left turn lane to Larsen Road. Because of the recently announced and funded Tonkin Highway extension, this project is expected to be long term and the traffic volumes along South Western Highway are expected to reduce as at least the regional traffic will switch to Tonkin Highway.

Based on these factors, it is recommended that the existing development crossover on South Western Highway be retained in its current format until the planned upgrades to this section of the highway are confirmed, funded and implemented. Once the upgrades are completed, the existing crossover may be modified to a left in/left out configuration because of the proposed centre median.

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# **APPENDIX A**

# PROPOSED DEVELOPMENT SITE PLAN



# **APPENDIX B**

# **PARKING ASSESSMENT**

(LPS32)

**Table B1. Percentage of parking demand temporal analysis – Typical Friday** 

Time	Fast Food Outlet 1	Fast Food Outlet 2	Motor Vehicle Repair	Motor Vehicle Wash	Service station
6:00	10%	10%	0%	0%	30%
7:00	10%	10%	0%	0%	30%
8:00	10%	10%	100%	10%	30%
9:00	20%	20%	100%	20%	60%
10:00	20%	20%	70%	50%	60%
11:00	50%	50%	70%	80%	60%
12:00	80%	80%	70%	80%	100%
13:00	90%	90%	70%	70%	100%
14:00	90%	90%	70%	70%	100%
15:00	80%	80%	90%	70%	100%
16:00	70%	70%	50%	70%	60%
17:00	60%	60%	30%	60%	30%
18:00	70%	70%	0%	50%	60%
19:00	80%	80%	0%	20%	30%
20:00	30%	30%	0%	10%	30%
21:00	10%	10%	0%	10%	30%

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Table B2. Percentage of parking demand temporal analysis – Typical Saturday

Time	Fast Food Outlet 1	Fast Food Outlet 2	Motor Vehicle Repair	Motor Vehicle Wash	Service station
6:00	10%	10%	0%	0%	30%
7:00	10%	10%	0%	0%	30%
8:00	10%	10%	80%	0%	30%
9:00	20%	20%	80%	10%	60%
10:00	20%	20%	70%	30%	60%
11:00	70%	70%	70%	60%	60%
12:00	80%	80%	50%	80%	100%
13:00	90%	90%	0%	90%	100%
14:00	80%	80%	0%	90%	100%
15:00	80%	80%	0%	90%	100%
16:00	50%	50%	0%	100%	60%
17:00	60%	60%	0%	80%	60%
18:00	70%	70%	0%	60%	60%
19:00	100%	100%	0%	50%	30%
20:00	70%	70%	0%	40%	30%
21:00	50%	50%	0%	20%	30%

Table B3. Actual parking demand temporal analysis – Typical Friday

Time	Fast Food Outlet 1	Fast Food Outlet 2	Motor Vehicle Repair	Motor Vehicle Wash	Service Station	Total demand	Parking surplus/ shortfall
6:00	2	4	0	0	1	7	71
7:00	2	4	0	0	1	7	71
8:00	2	4	16	0	1	23	55
9:00	4	7	16	1	2	30	48
10:00	4	7	11	2	2	27	51
11:00	11	18	11	4	2	45	33
12:00	18	28	11	4	3	63	15
13:00	20	32	11	3	3	69	9
14:00	20	32	11	3	3	69	9
15:00	18	28	14	3	3	66	12
16:00	15	25	8	3	2	53	25
17:00	13	21	5	3	1	43	35
18:00	15	25	0	2	2	44	34
19:00	18	28	0	1	1	47	31
20:00	7	11	0	0	1	18	60
21:00	2	4	0	0	1	7	71

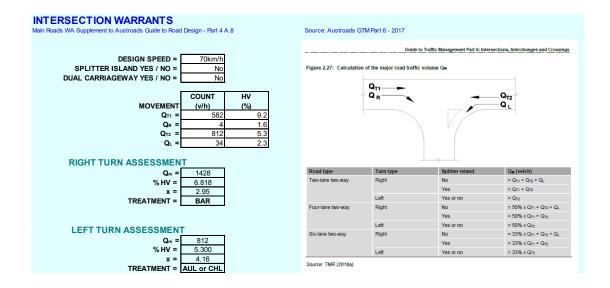
Table B4. Actual parking demand temporal analysis – Typical Saturday

Time	Fast Food Outlet 1	Fast Food Outlet 2	Motor Vehicle Repair	Motor Vehicle Wash	Service Station	Total demand	Parking surplus/ shortfall
6:00	2	4	0	0	1	7	71
7:00	2	4	0	0	1	7	71
8:00	2	4	13	0	1	19	59
9:00	4	7	13	0	2	26	52
10:00	4	7	11	1	2	26	52
11:00	15	25	11	3	2	56	22
12:00	18	28	8	4	3	60	18
13:00	20	32	0	4	3	58	20
14:00	18	28	0	4	3	53	25
15:00	18	28	0	4	3	53	25
16:00	11	18	0	4	2	35	43
17:00	13	21	0	4	2	40	38
18:00	15	25	0	3	2	44	34
19:00	22	35	0	2	1	60	18
20:00	15	25	0	2	1	43	35
21:00	11	18	0	1	1	30	48

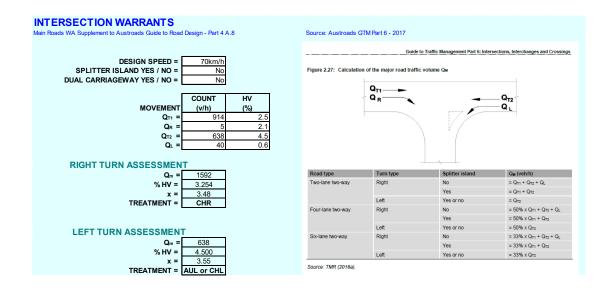
# **APPENDIX B**

# **TURN LANE ASSESSMENTS**

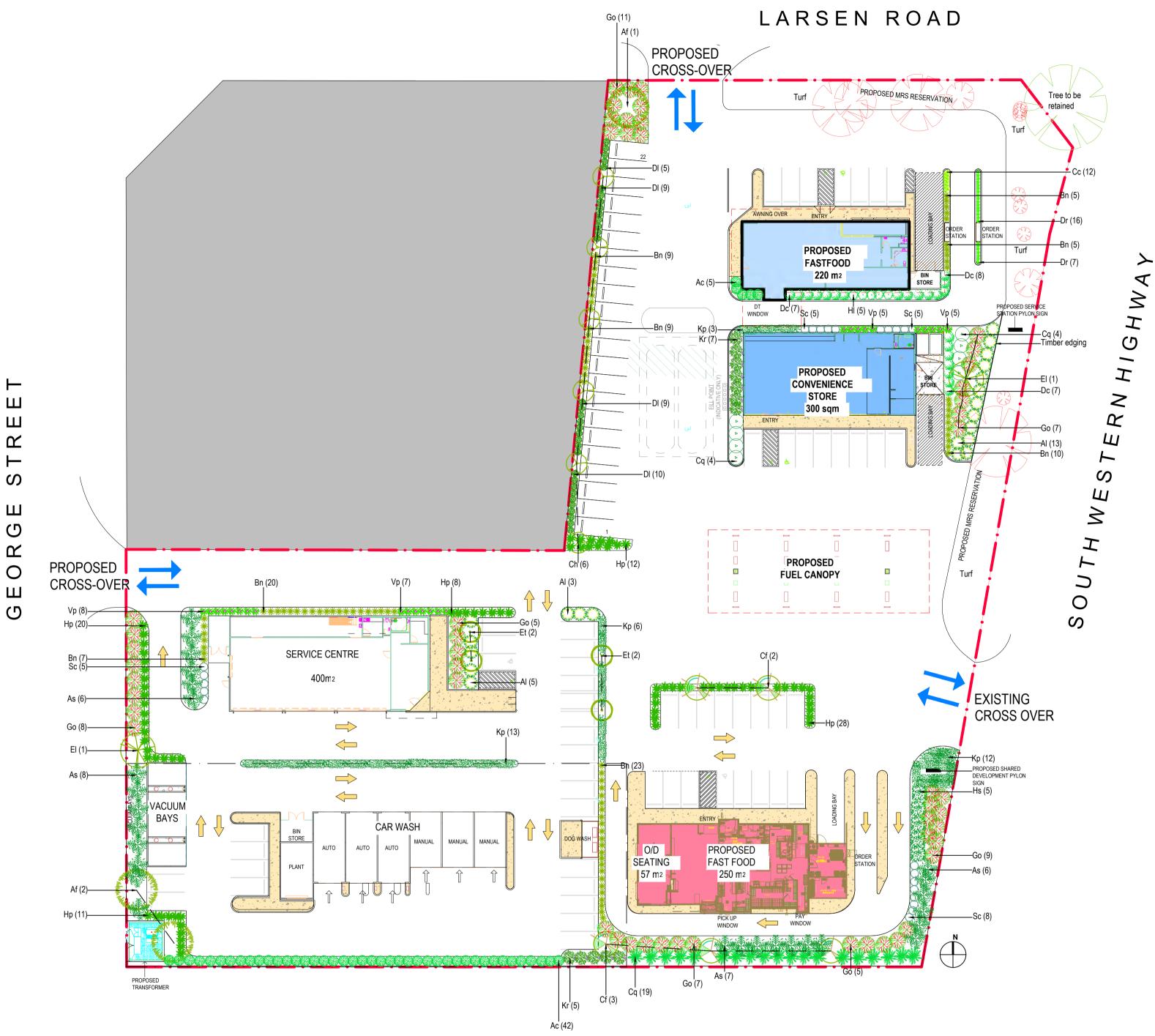
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## Turn lane assessment for the AM peak hour



Turn lane assessment for the PM peak hour



# INSTALLATION SPECIFICATIONS

# 1. TREE AND PLANT MATERIAL SUPPLY AND PLANTING

- 1.1 PLANT MATERIAL
- ALL PLANT STOCK SUPPLIED BY CONTRACTOR SHALL BE OF THE SPECIES AND SIZES AS THOSE ON THE PLANT SCHEDULE. SHOULD THERE BE ANY DIFFICULTIES IN SOURCING PLANTS, THE CONTRACTOR SHALL RECOMMEND SIMILAR SUITABLE SUBSTITUTE SPECIES AND/OR SIZES TO THOSE SHOWN ON THE DRAWINGS. NO SUBSTITUTIONS SHALL TAKE PLACE WITHOUT WRITTEN APPROVAL BY THE SUPERINTENDENT.
- GREENLIFE AND TURF MUST BE WELL KEPT: DELIVERED TO SITE ON DAY OF INSTALLATION, OUT OF FULL SUN, AWAY FROM ANIMALS AND PESTS AND ROOTS NOT ALLOWED TO DRY OUT AND SHALL:
  - BE TRUE TO SPECIES, SUBSPECIES AND VARIETY -BE IN FIRST CLASS CONDITION AND HEALTHY -BE OF GOOD FORM CONSISTENT WITH SPECIES AND VARIETY -AND BE PLANTED AS PER THE INSTRUCTIONS BELOW.
- 1.2. GENERAL PLANTING INSTRUCTIONS
- SETTING OUT OF WORKS WHERE UNDERGROUND SERVICES, MANHOLES, CABLE PITS, KERBING, PAVING AND OTHER OBSTRUCTIONS OCCUR, PLANT CLEAR OF SUCH SERVICES AND OBSTRUCTIONS AND PROTECT SERVICES AND OBSTRUCTIONS FROM DAMAGE BY MACHINES AND
- REMOVE ALL PLANTS FROM THEIR CONTAINERS, IN SUCH A MANNER AS TO DO AS LITTLE DISTURBANCE AS POSSIBLE TO THE ROOTS. WHERE NECESSARY, TEASE OUT ROOT-BALLS BEFORE PLANTING. PLACE TREES, SHRUBS AND PLANTS IN HOLES IN AN UP-RIGHT POSITION AND BACKFILL LEVEL WITH TOP OF ROOT-BALL. COMPACT SOIL BY HAND.
- REFER DETAILS 'TYPICAL TREE PLANTING' AND 'TYPICAL SHRUB
- A ROOT BARRIER IS TO BE INSTALLED FOR ALL TREES.
- 1.3 SOIL CONDITIONER

FOUIPMENT

 AFTER SITE WORKS AND BEFORE PLANTING SUPPLY AND INSTALL TO ALL PLANTING AREAS SOIL CONDITIONER

- PRIOR TO PLACEMENT ENSURE ALL BASE MATERIAL IS CLEAN, FREE DRAINING AND FREE OF ALL BUILDER'S RUBBLE, RUBBISH, DELETERIOUS MATERIAL AND CONTAMINATION. ALL AREAS CONTAMINATED BY THE BUILDER OR OTHERS SHALL BE REMOVED AND REPLACE WITH CLEAN FILL SAND TO THE APPROVAL OF THE SUPERINTENDENT.
- PLACE SOIL CONDITIONER TO A DEPTH OF 15MM OVER THE FULL EXTENT OF AREAS TO BE CONDITIONED. ROTARY-HOE OR SPADE DIG WHERE NECESSARY, SOIL CONDITIONER INTO EXISTING SITE SOIL TO A DEPTH OF 80MM TO PRODUCE A FULLY HOMOGENEOUS MIX. REMOVE ALL RUBBLE OR OTHER EXTRANEOUS AND DELETERIOUS MATTER EXPOSED AS A RESULT OF CULTIVATION, INCLUDING ANY BASE COURSE MATERIAL.
- SOIL CONDITIONER SHALL COMPLY WITH AS4454COMPOSTS, SOIL CONDITIONERS AND MULCHES.
- 1.4 FERTILISING
- AFTER PLANTING AND AT TIME OF BACK FILLING ALL PLANTS ARE TO RECEIVE APPROVED PROPRIETY ITEM OF EIGHT TO NINE MONTH SLOW-RELEASE FERTILISER SUITABLE FOR AUSTRALIAN NATIVE PLANTS.
- FERTILIZER TO BE APPLIED IN BACKFILL (BELOW GROUND) DURING PLANTING AT THE MANUFACTURERS' RECOMMENDED RATE FOR THE RELATIVE PLANT SIZE, AND AT A MINIMUM RATE AS FOLLOWS: - 30 LITRE POT SIZE PLANTS TO HAVE FOURTY GRAMS - 13CM - 14CM POT SIZE PLANTS TO HAVE TEN GRAMS

# 2.1 MINOR PREPARATION

- REMOVE ALL RUBBISH, ROOTS AND STONES GREATER THAN 10MM IN DIAMETER TO A DEPTH OF 300MM AND GRADE TO EVEN GRADES. GRADE OUT ALL DEPRESSIONS AND HUMPS LESS THAN 150MM FROM THE GENERAL GRADE.
- ALL SURFACES PREPARED FOR GRASSING TO FINISH FLUSH WITH ADJOINING KERBS TO ROADS, PARKING AND PAVED AREAS, AND WITH FOOT PAVEMENTS, MOWING STRIPS, MANHOLES, PIT AND THE LIKE. WHERE PLUMBING CONNECTOR TRAPS AND RAINWATER RELIEF OVERFLOWS OCCUR, FINISH GROUND LEVEL 75MM BELOW OVERFLOW LEVEL. ALL GRADING WORKS SHALL BE UNDERTAKEN BY HAND WORK OR BY MACHINE AS IS APPROPRIATE TO THE WORK HOWEVER ALL GRADING AND EARTHWORKS WITHIN A DISTANCE OF 600MM RADIUS OF

- SPRINKLERS OR OTHER FIXED RETICULATION APPARATUS SHALL BE HAND WORKED TO PREVENT DAMAGE TO EQUIPMENT. NO IRREGULARITIES, DEPRESSIONS, HOLLOWS OR ABRUPT CHANGES IN GRADES OR FALLS WILL BE ACCEPTED.
- 2.2 FERTILISING PRIOR TO TURF LAYING SUPPLY AND SPREAD TO THE FULL EXTENT OF AREA TO BE TURFED PELLETISED ORGANIC FERTILIZER EQUAL OR EQUIVALENT TO "DYNAMIC LIFTER" AT THE RATE OF 100 GRAMS PER SQUARE METRE TO THE APPROVAL OF THE SUPERINTENDENT.
- 2.3 WATERING BEFORE COMMENCING PLANTING, ENSURE ADEQUATE WATERING SERVICES AND EQUIPMENT ARE AVAILABLE AND PROPERLY
- AREAS TO BE PLANTED SHALL FIRST BE WATERED TO A DEPTH OF 100MM AND THE PLANTING SHALL BE CARRIED OUT IMMEDIATELY AFTER
- THROUGHOUT THE CONTRACT UP TO PRACTICAL COMPLETION, WATERING SHALL BE PROPERLY UNDERTAKEN, EITHER BY HAND OR IRRIGATION SYSTEM TO KEEP THE PLANTED AREA MOIST TO A DEPTH OF 100MM AT NOT MORE THAN TWO (2) DAY INTERVALS EXCEPTING SATURDAYS, SUNDAYS AND PUBLIC HOLIDAYS UNLESS OTHERWISE DIRECTED BY THE SUPERINTENDENT.
- 2.4 TURF LAYING • LAY THE TURF ALONG THE LAND CONTOURS WITH STAGGERED, CLOSE BUTTED JOINTS, AND SO THAT THE FINISHED TURF SURFACE FINISHES 20MM BELOW ADJACENT FINISHED SURFACES OF EDGING AND THE LIKE. AS SOON AS PRACTICABLE AFTER LAYING, ROLL THE TURF WITH A ROLLER WEIGHTING NOT MORE THAN 90 KG/M OR A PLATE COMPACTOR.
- 2.5 TOP DRESSING UNDERTAKE TOP DRESSING AS REQUIRED TO PRODUCE A TRUE AND EVEN SURFACE TO THE FULL EXTENT OF TURF AREAS FREE OF HUMPS, HOLLOWS AND DEPRESSIONS. SHOULD TOP DRESSING BE REQUIRED, UNDERTAKE WHEN THE TURF IS ESTABLISHED, MOW CLOSELY, REMOVE CUTTINGS AND LIGHTLY TOP DRESS TO A DEPTH OF 10MM WITH APPROVED QUALITY TOP DRESSING SAND. RUB THE DRESSING WELL INTO THE JOINS AND CORRECT ANY UNEVENNESS IN THE TURF SURFACE.

2.6 FERTILISING

- ONE WEEK AFTER LAYING TURF, APPLY TO THE WHOLE AREA A QUALITY
- PROPRIETARY BRAND FERTILISER. EVENLY SPREAD FERTILIZER AT THE RATE INDICATED ON PACKET AND IMMEDIATELY THOROUGHLY WATER IN.

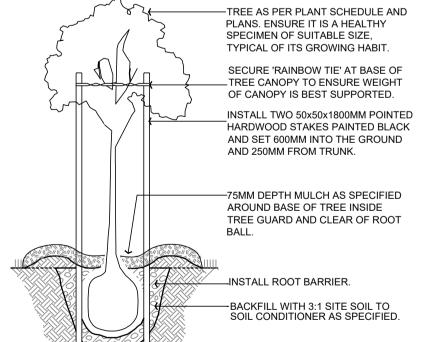
# 3. TIMBER EDGING

INSTALL EDGING AS INDICATED ON 'TIMBER EDGING DETAIL'.

- ALL MULCH SHALL MEET AUSTRALIAN STANDARD 4454-2012.
- SITE MULCH SHALL BE CHUNKY PINE BARK WOOD CHIPS. MULCH IS TO BE COMPLETELY FREE OF ALL NOXIOUS WEEDS, SEEDS
- AND FUNGUS, INSECT PESTS AND OTHER DELETERIOUS MATERIAL. ALL GARDEN BEDS AND TREE SURROUNDS TO BE MULCHED TO A
- MINIMUM DEPTH OF 75MM, KEEPING MULCH CLEAR OF PLANT STEMS. TIDY AND GRADE MULCH AFTER APPLICATION, FINISHING 20MM BELOW SURROUNDING HARD SURFACES.

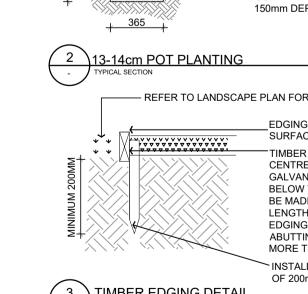
- ALL GARDEN BEDS TO BE IRRIGATED. INSTALL A SUB-MULCH DRIP SYSTEM FOR ALL GARDEN BEDS AND RECESSED SPRINKLERS FOR TURF
- CONTROLLER TO BE AUTOMATIC SYSTEM WITH RAIN SENSOR. LOCATION TO BE CONFIRMED ON SITE.
- THE CONTRACTOR IS RESPONSIBLE FOR LAYOUT DESIGN AND INSTALLATION OF IRRIGATION SYSTEM.
- AT TIME OF COMPLETION THE IRRIGATION SYSTEM SHALL BE FULLY AUTOMATED, WORKING EFFICIENTLY AND EFFECTIVELY AND WATERING TIMES PROGRAMMED.

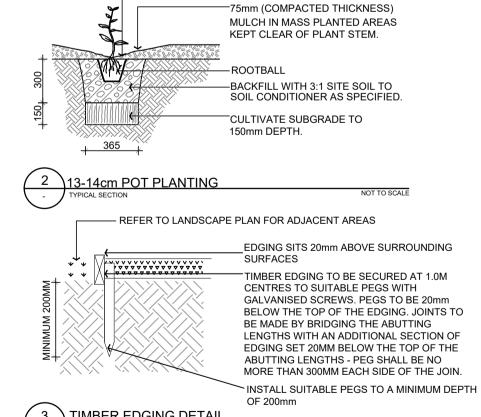
	PLANT	SCHEDULE A	ND SYMB	OL LEGEND						
Code on plan	Symbol	Botanic Name	Mature height x width	Minimum installation size	Number					
TREES						TREE VAR	RIETIES			
Af	The same of the sa	Agonis flexuosa	6-8m x 5-6m*	30 Litre	3					
Ch	$\bigcirc$	Callistemon hybrid 'Kings Park Special'	4m x 3m	30 Litre	6	Agonis flexuosa	Callistemon hybrid 'Kings	Corymbia ficifolia 'Late	Eucalyptus	
Cf		Corymbia ficifolia 'Late Red Flowering Gum'	5m x 4m	30 Litre	5			Red Flowering Gum'		
El		Eucalyptus lane-poolei	8m x 5m	30 Litre	2					
Et	$\odot$	Eucalyptus torquata	5m x 3m	30 Litre	4	Eucalyptus torquata				
SHRUBS						SHRUB VA	RIETIES			
Ac		Adenanthos cygnorum	2m x 1.5m	13cm	47					
Bn	*	Banksia nivea	80cm x 1m	13cm	88	Adenanthos	Banksia	Calothamnus	Darwinia	
Cq	*	Calothamnus quadrifidus	2.5m x 2.5m	13cm	19	cygnorum	nivea		citriodora	
Dc		Darwinia citriodora	1.5m x 1.5m	13cm	22					
Н	THE STANKE OF TH	Hakea lissocarpha	1.5m x 1.5m	13cm	5	Hakea	Kunzea	Verticordia		
Kr		Kunzea recurva	2m x 2m	13cm	12	lissocarpha	recurva	plumosa		
Vp		Verticordia plumosa	60cm x 1m	13cm	25					
GRASSES						GRASS VA	RIETIES _			
Сс		Conostylus candicans	30cm x 50cm	13cm	12	AND BY THE PROPERTY OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED	Conostylus		anella revoluta	
Dr		Dianella revoluta 'Revelation'	50cm x 50cm	13cm	23		candicans	'Re	evelation'	
GROUND C					_	GROUND (	COVER VAR	RIETIES		
Al	Wallson S.	Acacia lasiocarpa prostrate	30cm x 2m	13cm	21	200				
As		Acacia saligna prostrate	30cm x 3m	13cm	27					1
Cqp	\$.	Calothamnus quadrifidus prostrate	60cm x 2m	13cm	8	Acacia		a Calothamnus		Grevill
DI		Dampiera linearis 'Blue'	30cm x 1m	13cm	33	lasiocarpa prostrate	prostrate	quadrifidus prostrate	linearis 'Blue'	obtusi 'Gin G
Go		Grevillea obtusifolia 'Gir Gin Jewel'	50cm x 2.5m	13cm	52					Jewel'
Нр	*	Hemiandra pungens 'Alba'	30cm x 1.5m	13cm	79					
Hs		Hibbertia scandens	30cm x 2m	13cm	5	Hemiandra	Hibbertia	Kennedia	Scaevola	
Кр		Kennedia prostrata	10cm x 3m	13cm	34	pungens	scandens	prostrata	calliptera	
Sc	0	Scaevola calliptera	40cm x 1.2m	13cm	23	- 'Alba'				
TURF - appro	oximately 675n	n²			•	1				
As indicated		Kikuyu		Roll on	Site measure					
TOTAL PL	ANTS				555					
		EXISTING TRE	E LEGEN	D						
Ę	3	Trees to be removed (	13)							



**TYPICAL DRAWINGS** 

DIAMETER OF ROOT





FORM RETENTION DISH

AROUND STEM.



DEVELOPMENT APPLICATION DEVELOPMENT APPLICATION

ion/issue description PROPOSED MIXED USE COMMERCIAL DEVELOPMENT LANDSCAPE PLAN 3 LARSON ROAD, BYFORD URBAN RETREAT GARDEN DESIGN 1:400 23275 COMMERCIAL AND RESIDENTIAL LANDSCAPE DESIGN SERVICES

E:amelia@urbanre
M:0438 926 313



# **CAPITAL PRUDENTIAL**

# COMMERCIAL DEVELOPMENT 3 LARSEN ROAD, BYFORD

# **ENVIRONMENTAL ACOUSTIC ASSESSMENT**

**NOVEMBER 2023** 

OUR REFERENCE: 31869-2-23358

## **DOCUMENT CONTROL PAGE**

# ENVIRONMENTAL ACOUSTIC ASSESSMENT 3 LARSEN ROAD, BYFORD

Job No: 23358

Document Reference: 31869-2-23358

FOR

# **CAPITAL PRUDENTIAL**

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Author:	Geoffrey Harris		Checked By:	Tim Reynolds	
Date of Issue:	15 November 2	2023			
		REVISION	HISTORY		
Revision	Description		Date	Author	Checked
1	Original Issue		15/11/23	GH	TR
2	Updated Plans		17/11/23	GH	TR
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# **APPENDICES**

A Site Layout – Master Plan

Herring Storer Acoustics
Our Ref: 31869-2-23358
Item 10.1.1 - Attachment 10

### 1. INTRODUCTION

Herring Storer Acoustics were commissioned by Capital Prudential to carry out an acoustic study with regards to compliance with the requirements of the Environmental Protection (Noise) Regulations 1997 for the proposed commercial development at 3 Larsen Road, Byford.

Based on information provided, noise emissions from associated with the operation of the development at 3 Larsen Road, Byford would meet the *Environmental Protection (Noise)* Regulations 1997.

This assessment contains details of noise associated with mechanical plant, fast food premises, car wash, deliveries, service station as well as car movements throughout the site.

#### 2. CRITERIA

The allowable noise level at the surrounding locales is prescribed by the *Environmental Protection (Noise) Regulations 1997*. Regulations 7 & 8 stipulate maximum allowable external noise levels determined by the calculation of an influencing factor, which is then added to the base levels shown below in Table 1. The influencing factor is calculated for the usage of land within two circles, having radii of 100m and 450m from the premises of concern.

**TABLE 1 - BASELINE ASSIGNED OUTDOOR NOISE LEVEL** 

Premises Receiving Noise	Time of Day	Assigned Level (dB)			
Fremises Receiving Noise	Time of Day	L <sub>A10</sub>	L <sub>A1</sub>	L <sub>Amax</sub>	
	0700 - 1900 hours Monday to Saturday (Day)	45 + IF	55 + IF	65 + IF	
	0900 - 1900 hours Sunday and Public Holidays (Sunday / Public Holiday Day Period)	40 + IF	50 + IF	65 + IF	
Noise sensitive premises	1900 - 2200 hours all days (Evening)	40 + IF	50 + IF	55 + IF	
	2200 hours on any day to 0700 hours Monday to Saturday and 0900 hours Sunday and Public Holidays (Night)	35 + IF	45 + IF	55 + IF	
Commercial premises	All Hours	60	75	80	

Note:  $L_{A10}$  is the noise level exceeded for 10% of the time.

L<sub>A1</sub> is the noise level exceeded for 1% of the time.

 $L_{\mbox{\scriptsize Amax}}$  is the maximum noise level.

IF is the influencing factor.

It is a requirement that received noise be free of annoying characteristics (tonality, modulation and impulsiveness), defined below as per Regulation 9.

"impulsiveness" means a variation in the emission of a noise where the difference between  $L_{Apeak}$  and  $L_{Amax\,Slow}$  is more than 15 dB when

determined for a single representative event;

"modulation" means a variation in the emission of noise that –

- (a) is more than 3dB L<sub>A Fast</sub> or is more than 3 dB L<sub>A Fast</sub> in any one-third octave band;
- (b) is present for more at least 10% of the representative assessment period; and
- (c) is regular, cyclic and audible;

#### "tonality"

means the presence in the noise emission of tonal characteristics where the difference between –

- (a) the A-weighted sound pressure level in any one-third octave band; and
- (b) the arithmetic average of the A-weighted sound pressure levels in the 2 adjacent one-third octave bands.

is greater than 3dB when the sound pressure levels are determined as  $L_{Aeq,T}$  levels where the time period T is greater than 10% of the representative assessment period, or greater than 8 dB at any time when the sound pressure levels are determined as  $L_{A Slow}$  levels.

Where the noise emission is not music, if the above characteristics exist and cannot be practicably removed, then any measured level is adjusted according to Table 2 below.

TABLE 2 - ADJUSTMENTS TO MEASURED NOISE LEVELS

Where <b>tonality</b> is present	Where <b>tonality</b> is present Where <b>modulation</b> is present	
+5 dB(A)	+5 dB(A)	+10 dB(A)

The nearest affected locations have been shown on Figure 1 and identified as:

- R1 Residential Premises to the North at 10 Larsen Road
- R2 Residential Premises to the North at 2-8 Larsen Road
- R1 Noise sensitive premises to the East on South Western Highway
- C4 Commercial Premises to the South
- R5 School to the East

The influencing factor at the residential premises R1 has been determined to be +3 dB;

18% commercial in inner circle; 2% commercial in outer circle; within 450m of South Western Highway.

The influencing factor at the residential premises R2 and R3 has been determined to be +7 dB;

18% commercial in inner circle; 2% commercial in outer circle; within 450m of South Western Highway.

The influencing factor at the residential premises R5 has been determined to be +2 dB;

within 450m of South Western Highway.



FIGURE 1 – AREA MAP

Accordingly, the Assigned Noise Levels are as per Table 3 below.

**TABLE 3 - ASSIGNED OUTDOOR NOISE LEVEL** 

Premises		Assig	ned Leve	l (dB)
Receiving Noise	Time of Day		L <sub>A1</sub>	L <sub>Amax</sub>
	0700 – 1900 hours Monday to Saturday	48	58	68
	0900 - 1900 hours Sunday and Public Holidays	43	53	68
R1	1900 – 2200 hours all days	43	53	58
	2200 hours on any day to 0700 hours Monday to Saturday and 0900 hours Sunday and Public Holidays	38	48	58
	0700 – 1900 hours Monday to Saturday	52	62	72
	0900 - 1900 hours Sunday and Public Holidays	47	57	72
R2, R3	1900 – 2200 hours all days	47	57	62
	2200 hours on any day to 0700 hours Monday to Saturday and 0900 hours Sunday and Public Holidays	42	52	62
	0700 – 1900 hours Monday to Saturday	47	57	67
	0900 - 1900 hours Sunday and Public Holidays	42	52	67
R5	1900 – 2200 hours all days	42	52	57
	2200 hours on any day to 0700 hours Monday to Saturday and 0900 hours Sunday and Public Holidays	37	47	57
Commercial Premises; C4	All Hours	60	75	80

Notes: L<sub>A10</sub> is the noise level exceeded for 10% of the time.

 $L_{\text{A1}}$  is the noise level exceeded for 1% of the time.

 $L_{\mbox{\scriptsize Amax}}$  is the maximum noise level.

Item 10.1.1 - Attachment 10

### 3. CALCULATED NOISE LEVELS

Based on information provided, we believe that the following scenarios are representative of the development.

Scenario 1: Mechanical Plant; Assessed against L<sub>A10</sub> for all hours.

> All mechanical plant operating simultaneously for accommodation and services. During the night time period, mechanical plant has been assumed to in "Night Mode". This would be considered conservative as diversity of operation would not necessarily have all pieces of plant operating simultaneously. Emissions have been

considered tonal and attract a +5 dB(A) penalty.

Scenario 2: Car Movements within Drive through; assessed against LA1 for all

hours.

Noise associated with individual car movements whilst in drive

through.

Scenario 3: Car Movements around site; assessed against  $L_{A1}$  for all hours.

Noise associated with individual car movements around the site.

Scenario 4: Car Door Closing; assessed against L<sub>Amax</sub> for all hours.

> Noise associated with an individual car door closing at the most critical location. Emissions have been considered impulsive and

attract a +10 dB(A) penalty.

Scenario 5: Car Engine Starts; assessed against L<sub>Amax</sub> for all hours.

Noise associated with an individual car start at the most critical

location.

Scenario 6: Service Centre Operations; assessed against L<sub>A10</sub> for all hours.

Noise associated with the operation of the service centre; doors

open.

Scenario 7: Car Wash; assessed against L<sub>A10</sub> for all hours.

Noise associated with car wash operations, all units operating

simultaneously, doors open.

Scenario 8: Delivery Trucks; assessed against L<sub>A1</sub> for all hours.

Noise associated with delivery of goods to loading docks.

The Environmental Protection (Noise) Regulations 1997 state that noise associated Note: with cars movements and cars starting are exempt from complying with the Regulations. However, noise emissions from car doors are not strictly exempt from the Regulations. As a result, door slams, engine starts and car movements on site have all been assessed.

To determine the noise at each receiver for each scenario, Sound Power Levels listed in Table 4 have been utilised.

**TABLE 4 – SOUND POWER LEVEL** 

Item	Sound Power Level dB(A)
Air conditioning Unit	68 (65 Night Mode)
Kitchen Exhaust	75
Glass Dropping in Bin	110 L <sub>AMax</sub>
Car Door Slam	87 L <sub>Amax</sub>
Car Start	85 L <sub>Amax</sub>
Car Movement	81 L <sub>A1</sub>
Delivery Truck	85 L <sub>A1</sub>
Vacuum Units – with acoustic hood	82
Self Carwash Water Jets	94
Auto Car Wash Equipment – No Doors	87
Dog Wash Unit	88

Using the above sound power level and development plans (Attached), modelling software "SoundPLAN" was utilised to calculate the noise highest noise level received at each of the premises, shown below, including any appropriate penalty. For brevity, the operations have only been assessed against the most stringent time period. Note, as there is a cumulative assessment for the car wash operations, tonality has been included into the modelled noise levels of Vacuum Units and Dog Wash Units.

**TABLE 5 – CALCULATED NOISE LEVELS** 

Location	Noise Level dB(A)							
Location	<b>S1</b>	<b>S2</b>	<b>S3</b>	<b>S4</b>	<b>S5</b>	S6	<b>S7</b>	<b>S8</b>
R1	33 [38]	33	34	40 [50]	38	17	36	30
R2	37 [42]	37	45	46 [56]	44	17	40	40
R3	35 [40]	35	35	39 [49]	37	37	40	32
C4	41 [46]	41	46	56 [66]	52	49	56	38
R5	23 [28]	23	23	28 [38]	26	24	33	19

### 4. ASSESSMENT

Tables 6 to 13 identify provide the assessment for each of the eight scenarios based on the information presented in Section 4.

TABLE 6 - ASSESSMENT OF SCENARIO 1 - MECHANICAL PLANT

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A10</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)		
R1	38	Night Time	38	Complies		
R2	42	Night Time	42	Complies		
R3	40	Night Time	46	Complies		
C4	46	Night Time	60	Complies		
R5	28	Night Time	37	Complies		

TABLE 7 – ASSESSMENT OF SCENARIO 2 – CAR MOVEMENTS IN DRIVE THROUGH

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A1</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	33	Night Time	48	Complies
R2	37	Night Time	52	Complies
R3	35	Night Time	56	Complies
C4	41	Night Time	75	Complies
R5	23	Night Time	47	Complies

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Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A1</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)			
R1	34	Night Time	48	Complies			
R2	45	Night Time	52	Complies			
R3	35	Night Time	56	Complies			
C4	46	Night Time	75	Complies			
R5	23	Night Time	47	Complies			

### TABLE 9 – ASSESSMENT OF SCENARIO 4 - CAR DOOR SLAMS

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>AMax</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	50	Night Time	58	Complies
R2	56	Night Time	62	Complies
R3	49	Night Time	66	Complies
C4	66	Night Time	80	Complies
R5	38	Night Time	57	Complies

### TABLE 10 – ASSESSMENT OF SCENARIO 5 - CAR ENGINE STARTS

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>Amax</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	38	Night Time	58	Complies
R2	44	Night Time	62	Complies
R3	37	Night Time	66	Complies
C4	52	Night Time	80	Complies
R5	26	Night Time	57	Complies

### TABLE 11 - ASSESSMENT OF SCENARIO 6 - SERVICE CENTRE

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A10</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	17	Night Time	38	Complies
R2	17	Night Time	42	Complies
R3	37	Night Time	46	Complies
C4	49	Night Time	60	Complies
R5	24	Night Time	37	Complies

#### TABLE 12 - ASSESSMENT OF SCENARIO 7 - CAR WASH

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A10</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	36	Night Time	38	Complies
R2	40	Night Time	42	Complies
R3	40	Night Time	46	Complies
C4	56	Night Time	60	Complies
R5	33	Night Time	37	Complies

### TABLE 13 – ASSESSMENT OF SCENARIO 8 – DELIVERY TRUCKS

Location	Assessable Noise Level, dB(A)	Applicable Times of Day	Applicable L <sub>A1</sub> Assigned Level (dB)	Exceedance to Assigned Noise Level (dB)
R1	30	Night Time	48	Complies
R2	40	Night Time	52	Complies
R3	32	Night Time	56	Complies
C4	38	Night Time	75	Complies
R5	19	Night Time	47	Complies

### 5. CONCLUSION

Based on the above, noise from the proposed development to the adjacent premises would comply with the *Environmental Protection (Noise) Regulations 1997* at their prescribed periods.

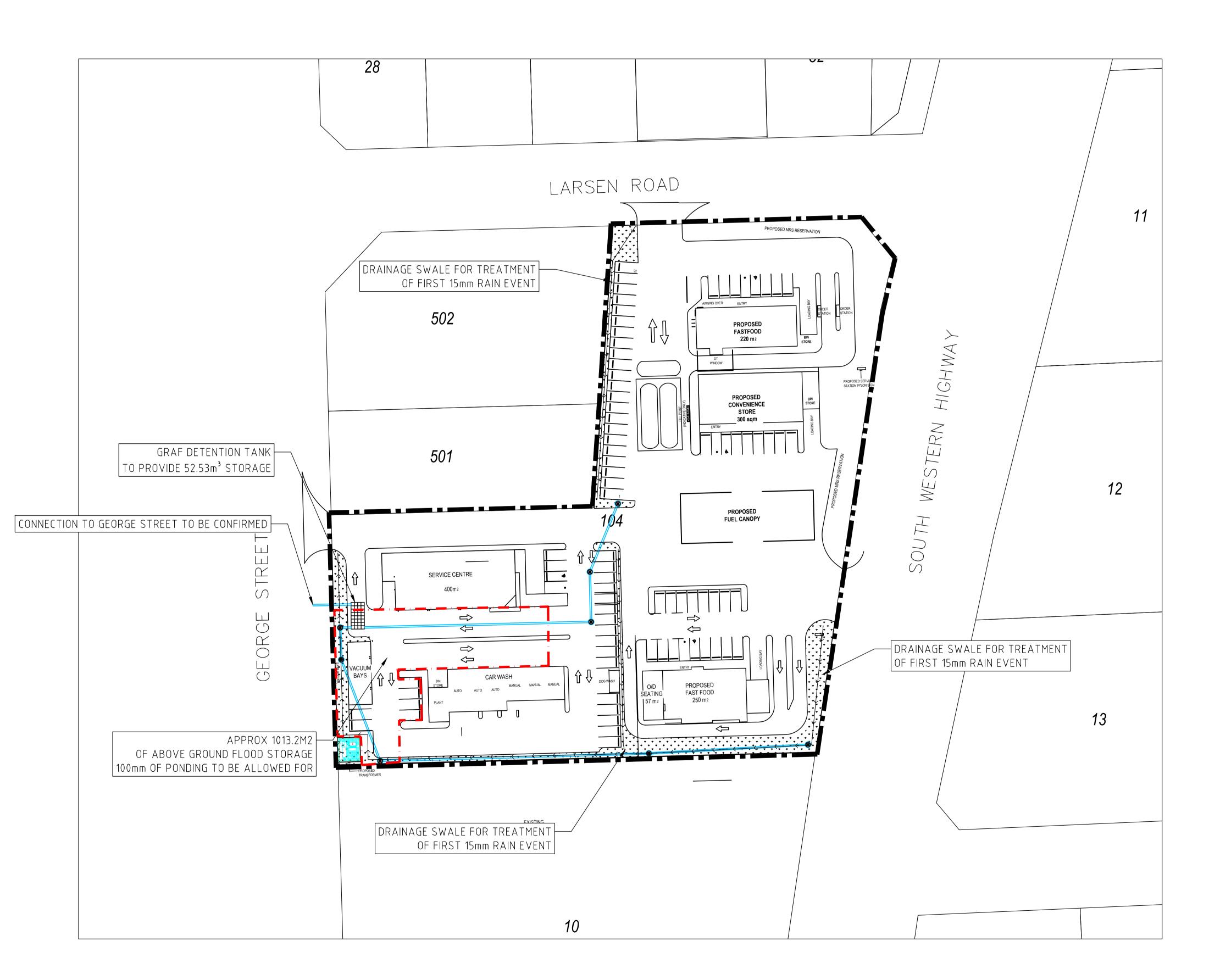
It is noted that hooded vacuum units were utilised for the assessment of the carwash, and it is recommended that, if possible, doors be closed on the Service Centre and Carwash where practicable to minimise noise spread.

Finally, specific mechanical plant section has note been made, and this report would require updating once this has been finalised to ensure that compliance is still met.

# **APPENDIX A**

**PLANS** 





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NOTES

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LEGEND

WORKS BOUNDARY

SWALE

ABOVE GROUND

STORAGE

# STORMWATER CALCULATION SUMMARY

SITE AREA: 11,630m<sup>2</sup>

FIRST 15mm RUNOFF TO BIORETENTION SWALES: 134.61m<sup>3</sup> SWALE STORAGE PROVIDED 350m<sup>3</sup>

PRE-DEVELOPMENT 10 YR ARI: 0.19 m³/s POST-DEVELOPMENT 10 YR ARI: 0.30 m³/s

PRE-DEVELOPMENT 100 YR ARI: 0.37m³/s

POST DEVELOPMENT 100 YR ARI: 0.58 m³/s

MINIMUM STORAGE REQUIRED FOR ATTENUATION 10YR ARI:

52.53m³ (TANK)

MINIMUM STORAGE REQUIRED FOR ATTENUATION 100YR ARI: 153.85m³ (CALCULATED AS A SUM OF BELOW STORAGES)

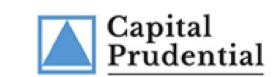
UNDERGROUND STORAGE REQUIRED: 52.53m³
ABOVE GROUND STORAGE/PONDING VOL REQUIRED: 101.32m³

1:500 AT A1 0 5m 10m 20m 30m

# NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	DRAWN	DATE
Α	ISSUED FOR INFORMATION	CF	23/11/23





DESIGNED:	DRAWN:	CHECKED:	
CF	CF	00	
SURVEY DATUM:	WAPC No:	SCALE:	
PCG94		AS SHOWN	@ A1
DWG IS NOT FOR CONSTRUC	TION UNLESS SIGNED BELOW:	DATE CREATED:	
		20/10/23	

3 LARSEN ROAD BYFORD, WA, 6122

PROPOSED MIXED USE DEVELOPMENT

# STORMWATER DRAINAGE PLAN

PROJECT NUMBER:	DRG NUMBER:	REV:
PC23356	CI-04.00 Ordrinary Council Meeting - 20 N	A May 2024



#### **Calculation Sheet**

Project3 Larsen RoadAuthorCFClientJack Bennet - Capital PrudentialApproverOODate19-Oct-23Doc Ref1RevisionA

#### 6.0 Post-Development

#### 6.1 Post-Development Catchment

Area (A)	1.16	ha	Input from 3.0 "Allowable Outflow"
Flow Length (L)	0.20	km	
Slope (S)	1.00	m	
310pe (3)	200.00	m	
Horton retardance (n)	0.01		
Fraction Impervious (f)	1.00		
ARI	10	yr	Input from 3.0 "Allowable Outflow"

# 6.2 Post-Development Runoff 7.0

Note: Flow rate calculation based on AR&R 1987 book VIII method.

Use this calculator to determine pre-development discharge (Allowable).

#### Q = CIA/360

$t_c$	8.00	min
C (Calculated)	0.90	
C (Engineers input)	0.90	
Q	0.30	m <sup>3</sup> /s

#### 6.4 Storage Volume

Design Infiltration Area	0.00	m²
Design Storage Volume	0.00	m³
Critical Duration	5	min
Minimum Storage Required	52.53	m³



# **Waste Management Plan**

3 Larsen Road, Byford

**Prepared for Capital Prudential Pty Ltd** 

10 January 2024

**Project Number: WMP24001** 



#### **DOCUMENT CONTROL**

Version	Description	Date	Author	Reviewer	Approver
1.0	First Approved Release	10/01/2024	AB	DP	AB

#### Approval for Release

Name	Position	File Reference
Ann Brouwer	Project Manager – Waste Management Consultant	WMP24001-01_Waste Management Plan_1.0
Signature		

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### **Executive Summary**

Capital Prudential Pty Ltd is seeking development approval for the proposed commercial development located at 3 Larsen Road, Byford (the Proposal).

To satisfy the conditions of the development application the Shire of Serpentine Jarrahdale (the Shire) requires the submission of a Waste Management Plan (WMP) that will identify how waste is to be stored and collected from the Proposal. Talis Consultants has been engaged to prepare this WMP to satisfy the Shire's requirements.

As demonstrated within this WMP, the Proposal will provide sufficiently sized Bin Storage Areas for storage of refuse and recyclables, based on the estimated waste generation volumes and suitable configuration of bins.

A private contractor will service the Proposal onsite, directly from the respective Bin Storage Areas. The private contractor's waste collection vehicle will enter and exit the Proposal in forward gear via Larsen Road or South Western Highway.

A building manager will oversee the relevant aspects of waste management at the Proposal.



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## **Diagrams**

Diagram 1: Bin Storage Areas

Diagram 2: Swept Path Analysis

# **Figures**

Figure 1: Locality Plan



#### 1 Introduction

Capital Prudential Pty Ltd is seeking development approval for the proposed commercial development located at 3 Larsen Road, Byford (the Proposal).

To satisfy the conditions of the development application the Shire of Serpentine Jarrahdale (the Shire) requires the submission of a Waste Management Plan (WMP) that will identify how waste is to be stored and collected from the Proposal. Talis Consultants has been engaged to prepare this WMP to satisfy the Shire's requirements.

The Proposal is bordered by Larsen Road to the north, South Western Highway to the east, commercial properties to the south and George Street to the west, as shown in Figure 1.

#### 1.1 Objectives and Scope

The objective of this WMP is to outline the equipment and procedures that will be adopted to manage waste (refuse and recyclables) at the Proposal. Specifically, the WMP demonstrates that the Proposal is designed to:

- Adequately cater for the anticipated volume of waste to be generated;
- Provide adequately sized Bin Storage Areas, including appropriate bins; and
- Allow for efficient collection of bins by appropriate waste collection vehicles.

To achieve the objective, the scope of the WMP comprises:

- Section 2: Waste Generation;
- Section 3: Waste Storage;
- Section 4: Waste Collection;
- Section 5: Waste Management; and
- Section 6: Conclusion.



#### 2 Waste Generation

The following section shows the waste generation rates used and the estimated waste volumes to be generated at the Proposal.

#### 2.1 Proposed Tenancies

The anticipated volume of refuse and recyclables is based on the floor area (m<sup>2</sup>) of the commercial tenancies at the Proposal. The Proposal consists of the following:

- Fast Food 01 220m²;
- Convenience Store 300m²;
- Fast Food 02 250m<sup>2</sup>;
- Car Wash 220m<sup>2</sup>; and
- Service Centre 400m<sup>2</sup>.

The Car Wash will have its own small internal bins between each vacuum bay which will be emptied into the bins within the Service Centre's Bin Storage Area for collection, and therefore has not been included as part of this report.

#### 2.2 Waste Generation Rates

In order to achieve an accurate projection of waste volumes for the Proposal, consideration was given to the City of Melbourne's *Guidelines for Waste Management Plans* (2021) and the City of Gosnells *Information Sheet — Waste Collection* as they contain contemporary estimates of waste generated from convenience stores, fast food tenancies, and shops (non-food).

Table 2-1 shows the waste generation rates which have been applied to the Proposal.

**Table 2-1: Waste Generation Rates** 

Tenancy Use Type	Guideline Reference	Refuse Recycling	
Tenancy Ose Type	Guideline Reference	Generation Rate	Generation Rate
Fast Food 01	Gosnells – Fast Food Outlet	150L/100m²/day	150L/100m²/day
Convenience Store	Melbourne – Convenience Store	300L/100m <sup>2</sup> /day	150L/100m <sup>2</sup> /day
Fast Food 02	Gosnells – Fast Food Outlet	150L/100m <sup>2</sup> /day	150L/100m <sup>2</sup> /day
Service Centre	Melbourne – Shops (non-food)	50L/100m <sup>2</sup> /day	50L/100m <sup>2</sup> /day

#### 2.3 Waste Generation Volumes

Waste generation is estimated by volume in litres (L) as this is generally the influencing factor when considering bin size, numbers and storage space required.

Waste generation volumes in litres per week (L/week) adopted for this waste assessment are shown in Table 2-2. It is estimated that the commercial tenancies at the Proposal will generate a total of 12,435L of refuse and 9,285L of recyclables each week.



**Table 2-2: Estimated Waste Generation** 

Commercial Tenancies	Area (m²)	Waste Generation Rate (L/100m²/day)	Waste Generation (L/week)
	Refuse		
Fast Food 01	220	150	2,310
Convenience Store	300	300	6,300
Fast Food 02	250	150	2,625
Service Centre	400	400	1,200
		Total	12,435
	Recyclables		
Fast Food 01	220	150	2,310
Convenience Store	300	150	3,150
Fast Food 02	250	150	2,625
Service Centre	400	50	1,200
		Total	9,285



### **3** Waste Storage

Waste materials generated within the Proposal will be collected in the bins located in the Bin Storage Areas, as shown in Diagram 1.

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Diagram 1: Bin Storage Areas

#### 3.1 Internal Transfer of Waste

To promote positive recycling behaviour and maximise diversion from landfill, internal bins will be available throughout each tenancy at the Proposal and between the vacuum bays at the Car Wash for the source separation of refuse and recycling.

These internal bins will be collected by the staff/cleaners and transferred to the respective Bin Storage Area for consolidation into the appropriate bins, as required. This internal servicing method may be conducted outside of main operational hours to mitigate disturbances to visitors.

All bins will be colour coded and labelled in accordance with Australian Standards (AS 4123.7) to assist visitors, staff and cleaners to dispose of their separate waste materials in the correct bins.



#### 3.2 Bin Sizes

Table 3-1 gives the typical dimensions of standard bins sizes that may be utilised at the Proposal. It should be noted that these bin dimensions are approximate and can vary slightly between suppliers.

**Table 3-1: Typical Bin Dimensions** 

Dimensions (m)		Bin Sizes	
Difficusions (III)	240L	660L	1,100L
Depth	0.730	0.780	1.070
Width	0.585	1.260	1.240
Height	1.060	1.200	1.330
Floor area (m²)	0.427	0.983	1.327

Reference: SULO Bin Specification Data Sheets

#### 3.3 Bin Storage Area Sizes

Each tenancy at the Proposal will have adequate space for the required number of bins, modelled utilising the estimated waste generation in Table 2-2, bin sizes in Table 3-1 and based on preferred collection frequencies of refuse and recyclables each week.

Bin requirements will be determined as the development becomes operational and the nature of the tenants and waste management requirements are known.

#### 3.4 Bin Storage Area Design

The design of the Bin Storage Areas will take into consideration:

- Smooth impervious floor sloped to a drain connected to the sewer system;
- Taps for washing of bins and Bin Storage Areas;
- Adequate aisle width for easy manoeuvring of bins;
- No double stacking of bins;
- Doors to the Bin Storage Areas self-closing and vermin proof;
- Doors to the Bin Storage Areas wide enough to fit bins through;
- Ventilated to a suitable standard;
- Appropriate signage;
- Undercover where possible and be designed to not permit stormwater to enter the drain;
- Located behind the building setback line;
- Bins not to be visible from the property boundary or areas trafficable by the public; and
- Bins are reasonably secured from theft and vandalism.

Bin numbers and storage space within the Bin Storage Areas will be monitored by the building manager during the operation of the Proposal to ensure that the number of bins and collection frequency is sufficient.



#### 4 Waste Collection

A private waste collection contractor will service bins at the Proposal at the preferred collection frequencies utilising a rear loader waste collection vehicle.

The private contractor's rear loader waste collection vehicle will service the bins onsite, directly from the Bin Storage Areas. The private contractor's rear loader waste collection vehicle will travel with left hand lane traffic flow on Larsen Road or South Western Highway and turn into the Proposal in forward gear, and pull up directly opposite the Bin Storage Areas for servicing, as shown in Diagram 2.

It is proposed that servicing may be conducted outside of normal operating hours to allow the waste collection vehicle to utilise the empty carpark for manoeuvring and mitigate impacts on local traffic movements during peak traffic hours.

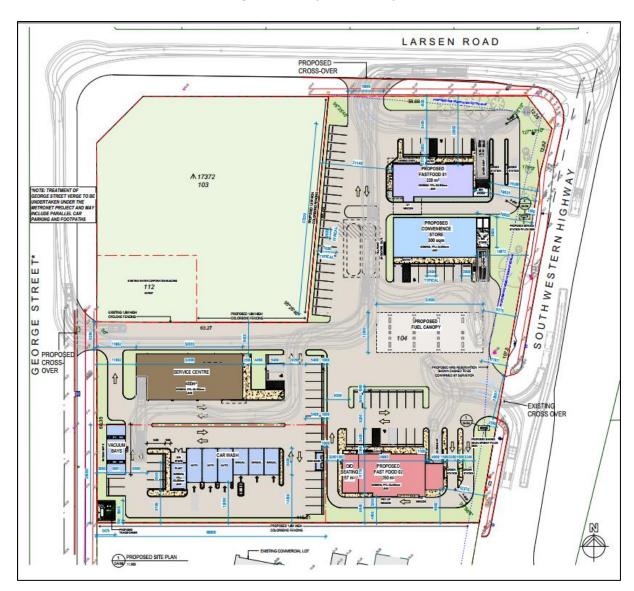
Private contractor's staff will ferry bins to and from the rear loader waste collection vehicle and the Bin Storage Areas during servicing. The private contractor will be provided with key/PIN code access to the Bin Storage Areas and security access gates to facilitate servicing, if required.

Once servicing is complete the private contractor's rear loader waste collection vehicle will exit in a forward motion, turning onto Larsen Road or South Western Highway.

The above servicing method will preserve the amenity of the area by removing the requirement for bins to be presented to the street on collection days. In addition, servicing of bins onsite will reduce the noise generated in the area during collection. Noise from waste vehicles must comply with the Environmental Protection (Noise) Regulations and such vehicles should not service the site before 7.00am or after 7.00pm Monday to Saturday, or before 9.00am or after 7.00pm on Sundays and Public Holidays.



**Diagram 2: Swept Path Analysis** 



#### 4.1 Bulk and Speciality Waste

Bulk and speciality waste materials will be removed from the Proposal as they are generated on an 'as required' basis. A temporary skip bin could be utilised for collections, if required. Bulk and speciality waste collection will be monitored by the building manager who will organise their transport to the appropriate waste facility, as required.



### **5** Waste Management

A building manager will be engaged to complete the following tasks:

- Monitoring and maintenance of bins and the Bin Storage Areas;
- Cleaning of bins and Bin Storage Areas, when required;
- Ensure all staff/cleaners at the Proposal are made aware of this WMP and their responsibilities thereunder;
- Monitor staff/cleaner behaviour and identify requirements for further education and/or signage;
- Monitor bulk and speciality waste accumulation and assist with its removal, as required;
- Regularly engage with staff/cleaners to develop opportunities to reduce waste volumes and increase resource recovery; and
- Regularly engage with the private contractors to ensure efficient and effective waste service is maintained.



### 6 Conclusion

As demonstrated within this WMP, the Proposal will provide sufficiently sized Bin Storage Areas for storage of refuse and recyclables, based on the estimated waste generation volumes and suitable configuration of bins.

A private contractor will service the Proposal onsite, directly from the Bin Storage Areas. The private contractor's waste collection vehicle will enter and exit the Proposal in forward gear via Larsen Road or South Western Highway.

A building manager will oversee the relevant aspects of waste management at the Proposal.



# **Figures**

Figure 1: Locality Plan





#### Assets | Engineering | Environment | Noise | Spatial | Waste

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